

UNIVERSITY OF BRIGHTON

School of the Environment

BEng CIVIL ENGINEERING

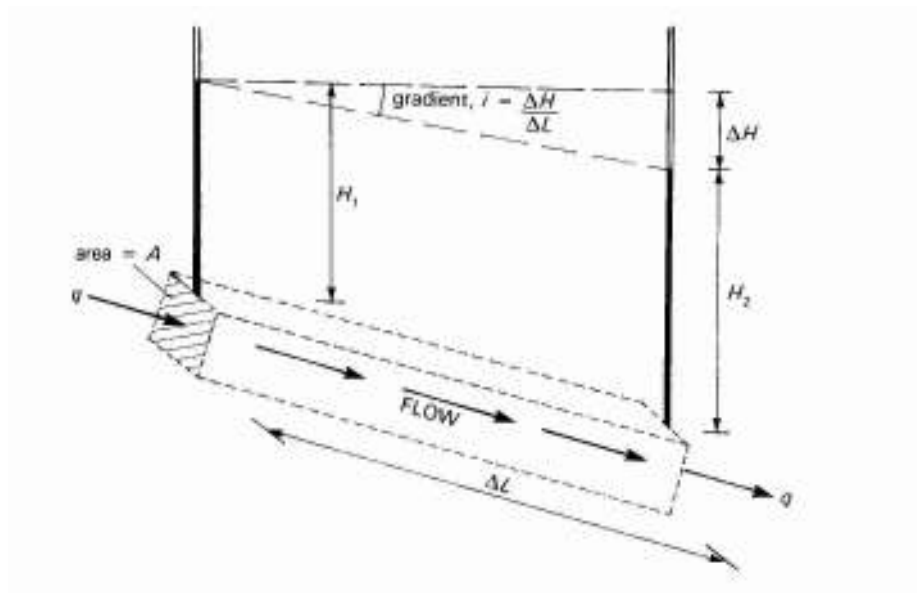
SOIL MECHANICS CN215

Formulae and Design Charts

PHASE RELATIONSHIPS

Term	Symbol	Units	Expression		Formulae
moisture content	w	%	$\frac{\text{mass water}}{\text{mass solids}}$	$\frac{m_w}{m_s}$	w is a fraction in formulae below
void ratio (partially saturated)	e	ratio	$\frac{\text{volume voids}}{\text{volume solids}}$	$\frac{V_a + V_w}{V_s}$	$e = \frac{n}{1-n} = \frac{wG_s}{S_r}$
void ratio (fully saturated)	e	ratio	$\frac{\text{volume water}}{\text{volume solids}}$	$\frac{V_w}{V_s}$	$e = wG_s$
porosity	n	ratio	$\frac{\text{volume voids}}{\text{total volume}}$	$\frac{V_a + V_w}{V_t}$	$n = \frac{e}{1+e} = \frac{wG_s}{S_r + wG_s}$
specific volume	v	ratio	$\frac{\text{total volume}}{\text{volume solids}}$	$\frac{V_a + V_w + V_s}{V_s}$	$v = 1 + e$
degree of saturation	S_r	%	$\frac{\text{volume water}}{\text{volume voids}}$	$\frac{V_w}{V_a + V_w}$	$S_r = \frac{\rho_w w G_s}{\rho_s G_s (1+w) - \rho_w} \times 100$
air voids content	A_v	%	$\frac{\text{volume air}}{\text{total volume}}$	$\frac{V_a}{V_t}$	$A_v = n(1 - S_r)$
particle density	ρ_s	Mg/m ³	$\frac{\text{mass solids}}{\text{volume solids}}$	$\frac{m_s}{V_s}$	$G_s \rho_w$
specific gravity	G_s	ratio	$\frac{\text{solids density}}{\text{water density}}$	$\frac{m_s}{V_s} \frac{1}{\rho_w}$	$\frac{\rho_s}{\rho_w}$
water density	ρ_w	Mg/m ³	$\frac{\text{mass water}}{\text{volume water}}$	$\frac{m_w}{V_w}$	$\rho_w = 1.0 \text{ Mg/m}^3$
bulk density (partially saturated)	ρ_b	Mg/m ³	$\frac{\text{total mass}}{\text{total volume}}$	$\frac{m_s + m_w}{V_a + V_w + V_s}$	$\rho_b = \frac{G_s(1+w)\rho_w}{1+e}$
bulk density (fully saturated)	ρ_{sat}	Mg/m ³	$\frac{\text{total mass}}{\text{total volume}}$	$\frac{m_s + m_w}{V_s + V_w}$	$\rho_{sat} = \frac{(G_s + e)\rho_w}{1+e}$
dry density	ρ_d	Mg/m ³	$\frac{\text{mass solids}}{\text{total volume}}$	$\frac{m_s}{V_t}$	$\rho_d = \frac{\rho_b}{1+w}$
bulk unit weight (partially saturated)	γ_b	kN/m ³	$\frac{\text{total weight}}{\text{total volume}}$	$\frac{m_t g}{V_t}$	$\gamma_b = \frac{G_s(1+w)\gamma_w}{1+e}$
bulk unit weight (fully saturated)	γ_{sat}	kN/m ³	$\frac{\text{total weight}}{\text{total volume}}$	$\frac{m_t g}{V_s + V_w}$	$\gamma_{sat} = \frac{(G_s + e)\gamma_w}{1+e}$
dry unit weight	γ_d	kN/m ³	$\frac{\text{weight solids}}{\text{total volume}}$	$\frac{m_s g}{V_t}$	$\gamma_d = \frac{\gamma_b}{1+w}$
unit weight water	γ_w	kN/m ³	$\frac{\text{weight water}}{\text{volume water}}$	$\frac{m_w g}{V_w}$	$\gamma_w = \rho_w g = 9.81 \text{ kN/m}^3$

PERMEABILITY AND FLOW



The quantity of flow through a given area in a unit time is therefore obtained as

$$q = kAi$$

Properties of a flow net:

Flow nets are constructed so that the intervals between adjacent equipotentials represent a *constant difference in head* (Δh) and the intervals between adjacent flow lines represent a *constant flow quantity* (Δq).

$$\begin{aligned} \text{So, the total head loss, } H &= \Delta h \times \text{no. equipotential intervals} \\ &= \Delta h \times N_e \end{aligned}$$

$$\begin{aligned} \text{and the total seepage flow, } q &= \Delta q \times \text{no. of flow intervals (channels)} \\ &= \Delta q \times N_f \end{aligned}$$

Isotropic material

$$q = k \Delta h \quad \text{per flow channel per unit length}$$

$$q = k \frac{H}{N_e} \quad \text{per flow channel per unit length}$$

H = total head difference

$$Q = k \frac{H}{N_e} N_f \quad \text{Total flow}$$

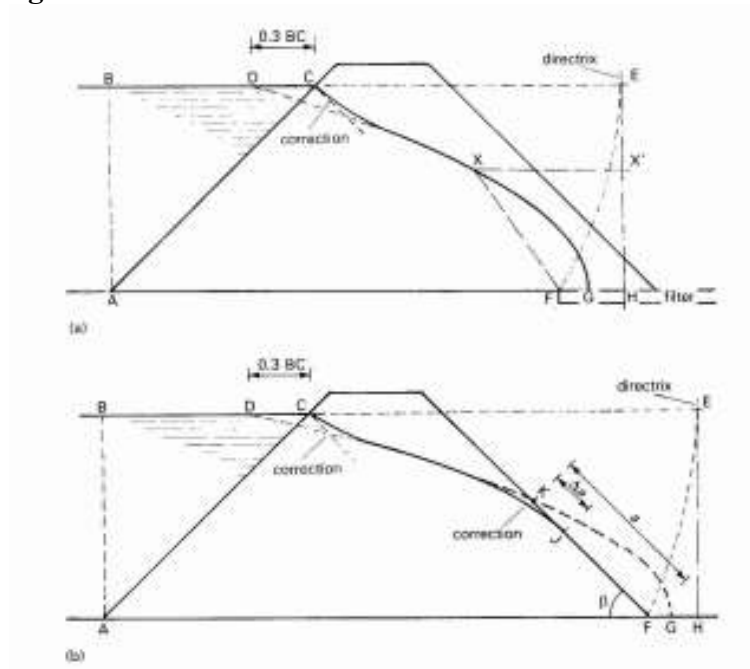
Anisotropic model $kh \neq kv$

$$k = k_x \sqrt{\frac{k_y}{k_x}} = \sqrt{k_x k_y}$$

Seepage quantity derived from a transformed flow nets;

$$Q = Ak \frac{N_f}{N_e} = A \frac{N_f}{N_e} \sqrt{k_x k_y}$$

Seepage through earth dams

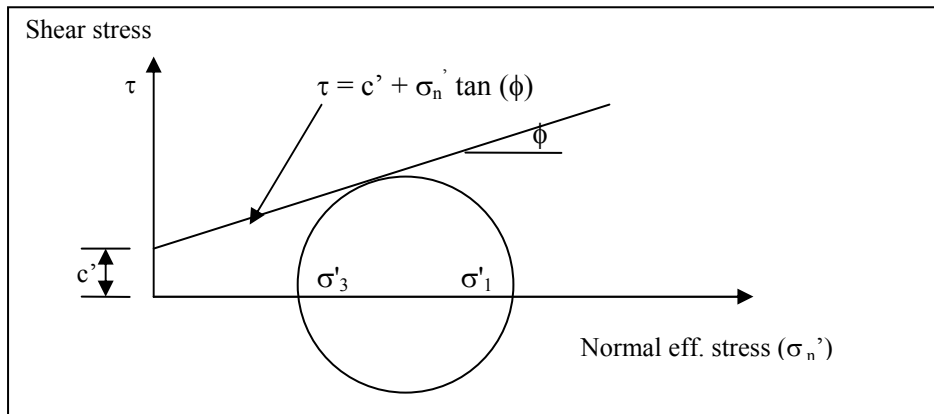


SHEAR STRENGTH

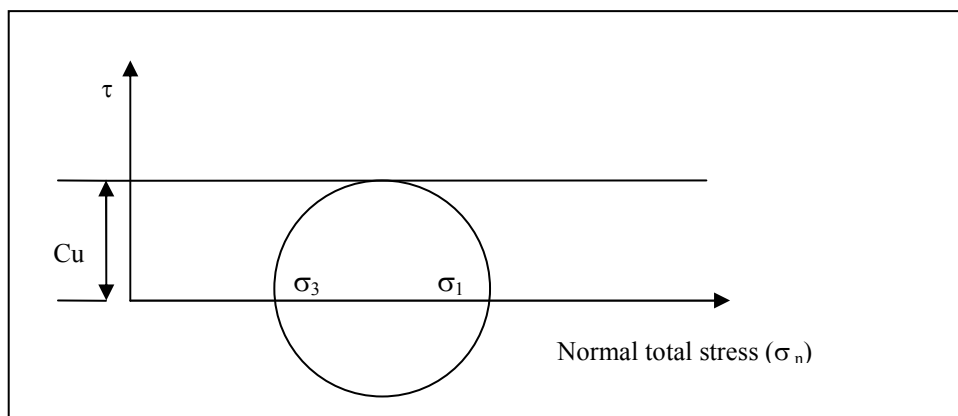
Coulomb's equation

$$\tau = c' + (\sigma_n - u) \tan \phi$$

$$\tau = c' + \sigma_n' \tan \phi$$



MOHR CIRCLE OF EFFECTIVE STRESS



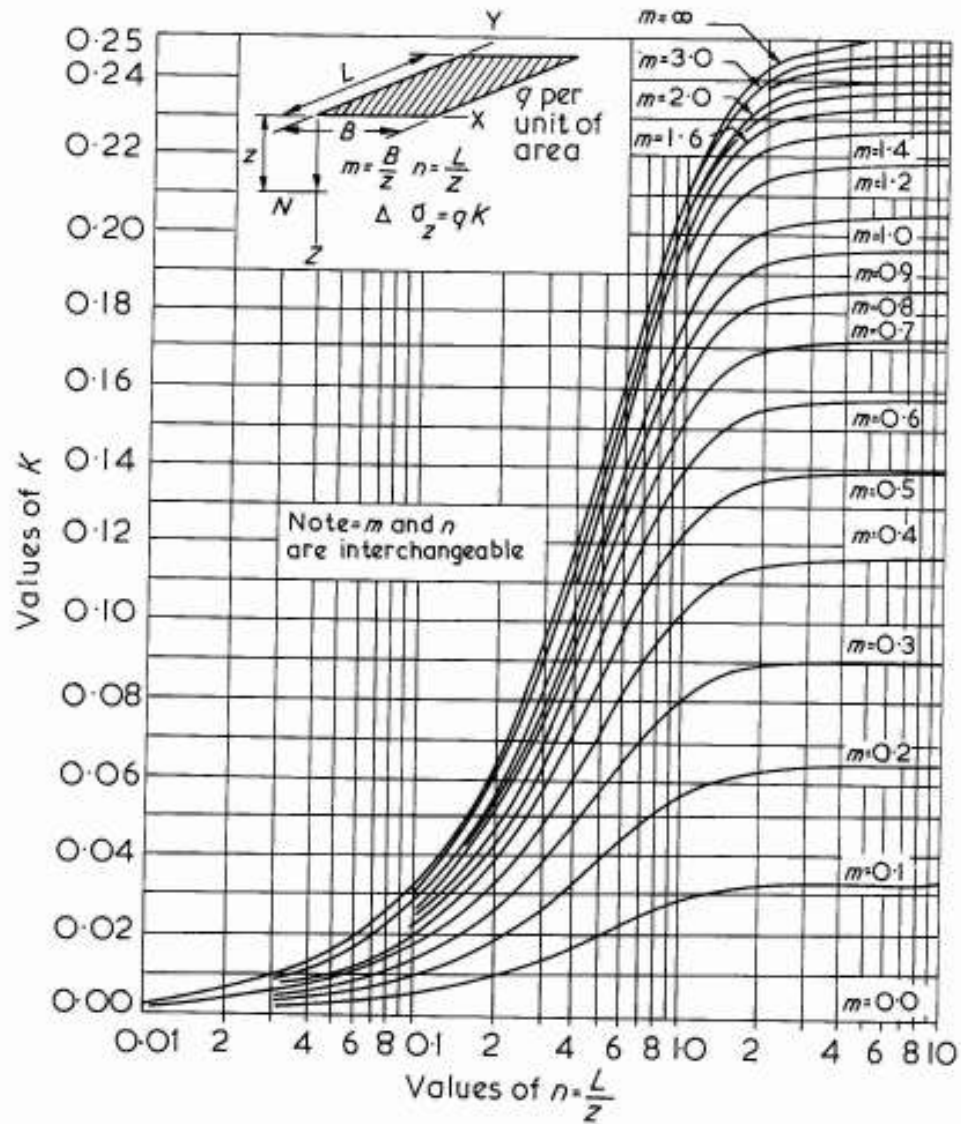
MOHR CIRCLE OF TOTAL STRESS

Deviator stress $q = \sigma_1 - \sigma_3$

Undrained shear strength $C_u = q/2$

STRESS DISTRIBUTION

Fadums Chart

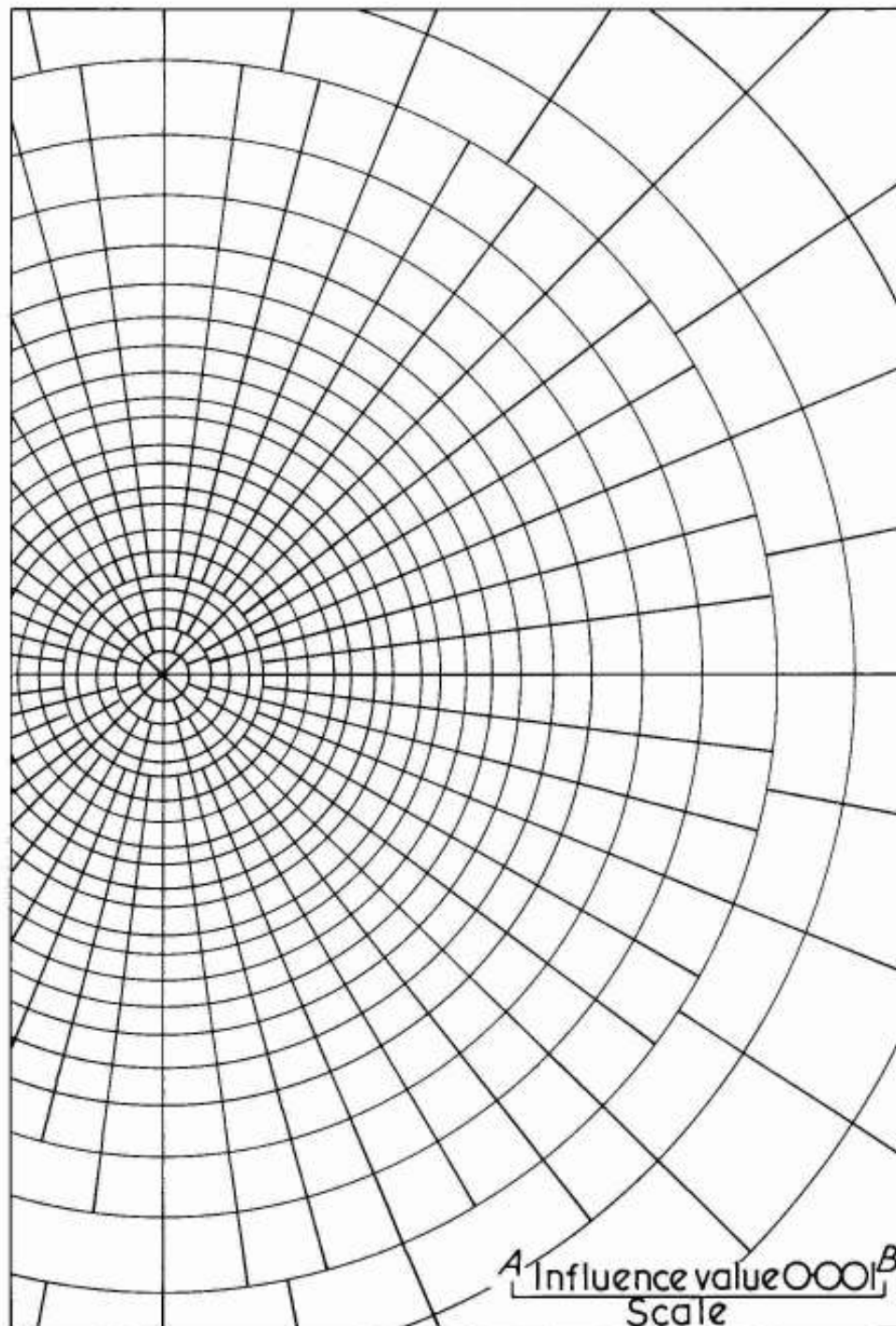


Newmark chart

For a uniform loading intensity of q the stress at the required depth below the point in question is computed as

$$\sigma_v = N \times I_N \times q$$

N is the number of segments or part segments, I_N is the chart influence value per field.



DETATCH AND SUBMIT WITH ANSWER PAPER