

Electromagnetics Theory

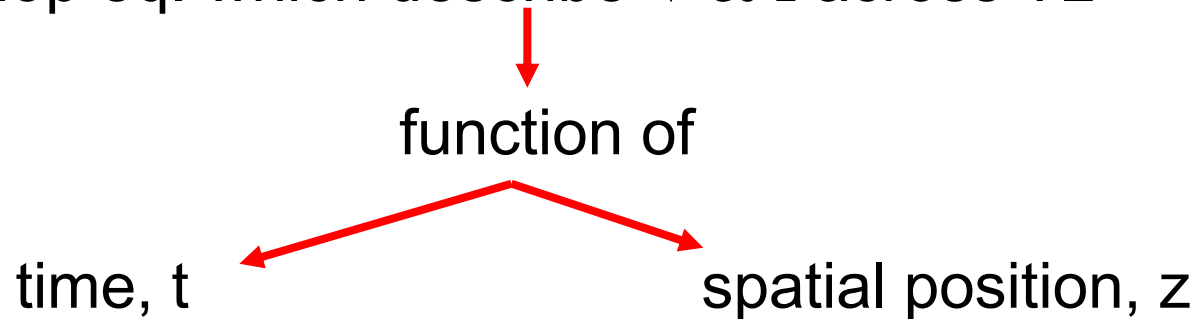
Transmission Line (Part 2)

Outline:

- 7.1 General Consideration
- 7.2 Lumped-Element model
- 7.3 Transmission line (TL) equation
- 7.4 Wave propagation on TL
- 7.5 Lossless TL
- 7.6 Input impedance of lossless line

7.3 Transmission line (TL) equation

- TL usually connects a source on one end and a load on the other end.
- Develop eq. which describe V & I across TL



- Telegrapher's eq. in phasor form: *Time-domain form of TL eq*

$$-\frac{d\tilde{V}(z)}{dz} = (R' + j\omega L')\tilde{I}(z) \quad \dots \quad (1)$$

$$-\frac{d\tilde{I}(z)}{dz} = (G' + j\omega C')\tilde{V}(z) \quad \dots \quad (2)$$

7.4 Wave propagation on TL

- By differentiating both side of eq (1) & (2) wrt z will give **Wave eq.** for $\tilde{V}(z)$ and $\tilde{I}(z)$, are given by

$$\frac{d^2\tilde{V}(z)}{dz^2} - \gamma^2\tilde{V}(z) = 0$$

$$\frac{d^2\tilde{I}(z)}{dz^2} - \gamma^2\tilde{I}(z) = 0$$

- γ is called the *complex propagation constant* of TL.

$$\gamma = \sqrt{(R' + j\omega L')(G' + j\omega C')}$$

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- γ consists of a real part α and imaginary part β .

$$\gamma = \alpha + j\beta$$

Attenuation constant
(Np/m)

Phase constant
(rad/m)

- With

$$\begin{aligned}\alpha &= \Re(\gamma) \\ &= \Re\sqrt{(R' + j\omega L')(G' + j\omega C')} \quad (\text{Np/m})\end{aligned}$$

$$\begin{aligned}\beta &= \Im(\gamma) \\ &= \Im\sqrt{(R' + j\omega L')(G' + j\omega C')} \quad (\text{Rad/m})\end{aligned}$$

Characteristic impedance (Z_0) of line:

is equal to the ratio of the voltage amplitude to the current amplitude for each of the traveling wave individually, but it is not equal to the ratio of total voltage $\tilde{V}(z)$ to the total current $\tilde{I}(z)$, unless one of the two wave is absent.

$$Z_0 = \frac{(R' + j\omega L')}{\gamma} = \sqrt{\frac{(R' + j\omega L')}{(G' + j\omega C')}}}$$

- $\alpha = 0$ \rightarrow *lossless line*
- $\alpha \neq 0$ \rightarrow *lossy transmission lines*

Exercise 3

An air line is a TL for which air is the dielectric material present between the two conductors, which renders $G'=0$. In addition, the conductors are made of a material with high conductivity so that $R'=0$. For an air line with characteristic impedance listed below, find the inductance per meter and the capacitance per meter of the line.

$$Z_0 = 50\Omega$$

$$\beta = 20\text{rad} / m$$

$$f = 700\text{MHz}$$

7.5 Lossless TL

- So far we have known two fundamental properties of transmission line
 - Propagation constant, γ
 - Characteristic impedance, Z_0
- Both are specified by the angular frequency ω and the line parameters R' , L' , G' and C'
- To minimize ohmic losses, we need to select conductors with very high conductivities ($R' \ll \omega L$) and dielectric materials with negligible conductivities ($G' \ll \omega C$), therefore allow us to set $R' = G' = 0$

- For lossless TL , $\alpha = 0$

- Where we know, $\gamma = \alpha + j\beta$

thus

$$\gamma = j\beta$$

$$= j\omega\sqrt{L'C'}$$

$$\alpha = 0$$

$$\beta = \omega\sqrt{L'C'}$$

$$Z_0 = \sqrt{\frac{L'}{C'}}$$

- relations for wavelength λ and phase velocity U_p with β

$$\lambda = \frac{2\pi}{\beta} = \frac{2\pi}{\omega\sqrt{L'C'}}$$

or

$$\beta = \omega\sqrt{\mu\varepsilon} \quad (\text{rad/m})$$

$$U_p = \frac{\omega}{\beta} = \frac{1}{\sqrt{L'C'}}$$

$$U_p = \frac{1}{\sqrt{\mu\varepsilon}} \quad (\text{m/s})$$

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- relation between λ and U_p is given by:

$$\lambda = \frac{u_p}{f} = \frac{c}{f} \frac{1}{\sqrt{\epsilon_r}} = \frac{\lambda_0}{\sqrt{\epsilon_r}}$$

$$\lambda_0 = \frac{c}{f}$$

Wavelength in air
corresponding to f

- In the case of TEM lossless medium, the phase velocity is independent of frequency, therefore its is a nondispersive medium.
- A nondispersive medium creates no distortion in transmitting data/ signal, due to the fact that all the phase velocity is the same for all the frequency components

Table 7-2: Characteristic parameters of transmission lines.

	Propagation Constant $\gamma = \alpha + j\beta$	Phase Velocity u_p	Characteristic Impedance Z_0
General case	$\gamma = \sqrt{(R' + j\omega L')(G' + j\omega C')}$	$u_p = \omega/\beta$	$Z_0 = \sqrt{\frac{(R' + j\omega L')}{(G' + j\omega C')}}$
Lossless ($R' = G' = 0$)	$\alpha = 0, \beta = \omega\sqrt{\epsilon_r}/c$	$u_p = c/\sqrt{\epsilon_r}$	$Z_0 = \sqrt{L'/C'}$
Lossless coaxial	$\alpha = 0, \beta = \omega\sqrt{\epsilon_r}/c$	$u_p = c/\sqrt{\epsilon_r}$	$Z_0 = (60/\sqrt{\epsilon_r}) \ln(b/a)$
Lossless two wire	$\alpha = 0, \beta = \omega\sqrt{\epsilon_r}/c$	$u_p = c/\sqrt{\epsilon_r}$	$Z_0 = (120/\sqrt{\epsilon_r}) \cdot \ln[(d/2a) + \sqrt{(d/2a)^2 - 1}]$ $Z_0 \simeq (120/\sqrt{\epsilon_r}) \ln(d/a),$ if $d \gg a$
Lossless parallel plate	$\alpha = 0, \beta = \omega\sqrt{\epsilon_r}/c$	$u_p = c/\sqrt{\epsilon_r}$	$Z_0 = (120\pi/\sqrt{\epsilon_r}) (d/w)$

Notes: (1) $\mu = \mu_0$, $\epsilon = \epsilon_r \epsilon_0$, $c = 1/\sqrt{\mu_0 \epsilon_0}$, and $\sqrt{\mu_0/\epsilon_0} \simeq (120\pi) \Omega$, where ϵ_r is the relative permittivity of insulating material. (2) For coaxial line, a and b are radii of inner and outer conductors. (3) For two-wire line, a = wire radius and d = separation between wire centers. (4) For parallel-plate line, w = width of plate and d = separation between the plates.

7.5.1 Voltage reflection coefficient

- Consider a transmission line of length l connected on one end to a generator circuit and on the other end to a load Z_L . The load is located at $z=0$ and the generator terminals are at $z=-l$

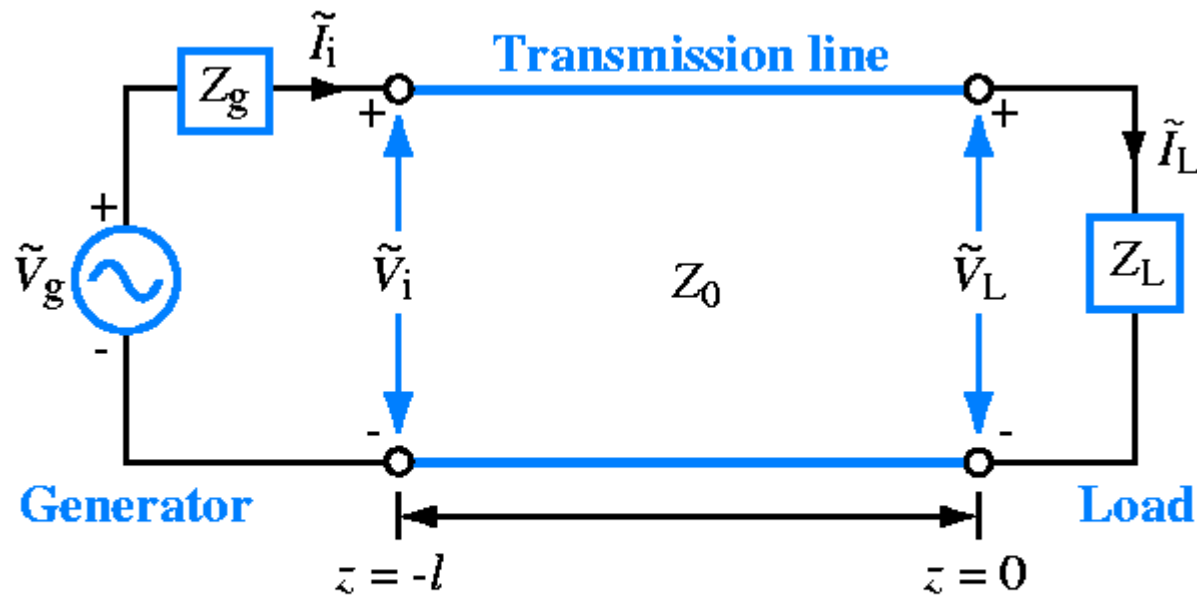


Figure 7-9

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- ‘ the ratio of the amplitude of the reflected voltage wave to the amplitude of the incident wave at the load is known as the *voltage reflection coefficient* Γ ‘

Voltage amplitude of incident wave

$$\Gamma = \frac{V_0^-}{V_0^+} = \frac{Z_L - Z_0}{Z_L + Z_0} = \frac{Z_L / Z_0 - 1}{Z_L / Z_0 + 1} \text{ (dimensionless)}$$

Voltage amplitude of reflected wave

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- the ratio of the current amplitudes is

$$\frac{I_0^-}{I_0^+} = -\frac{V_0^-}{V_0^+} = -\Gamma$$

- Note that Γ is governed by a single parameter, the load impedance Z_L , which is normalized to the characteristic impedance of the line Z_0 .

- Because Z_L is in general a complex quantity, hence Γ may also be complex:

$$\Gamma = |\Gamma| e^{j\theta_r}$$

Mag. Of
 $|\Gamma| \leq 1$

Phase angle

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- *a load is said to be matched to the line*

if $Z_L = Z_0$ because then there will be no reflection by the load ($\Gamma = 0$ and $V_0^- = 0$)'

- *when load is an open circuit* ($Z_L = \infty$)

$$\Gamma = 1 \quad \text{and} \quad V_0^- = V_0^+$$

- *when load is a short circuit* ($Z_L = 0$)

$$\Gamma = -1 \quad \text{and} \quad V_0^- = -V_0^+$$

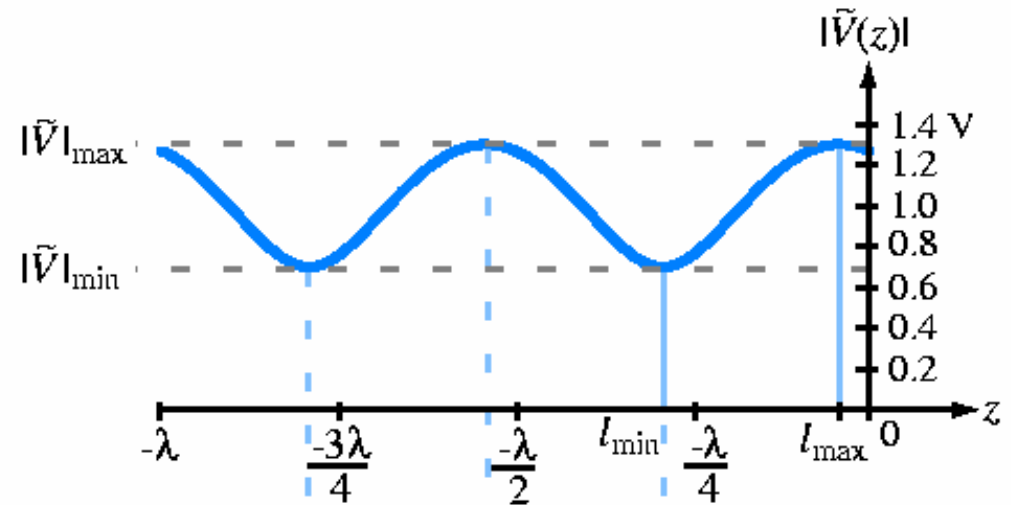
Exercise 4

A 100Ω transmission line is connected to a load consisting of a 50Ω resistor in series with a 10pF capacitor. Find the reflected coefficient at the load for a 100MHz signal.

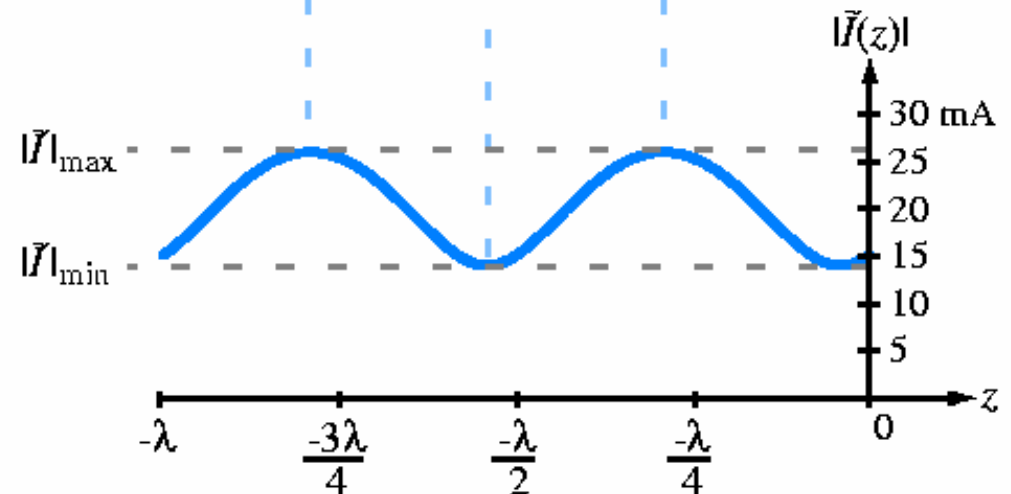
7.5.2 Standing Waves

- shows the standing-wave pattern for (a) $|\tilde{V}(z)|$ and (b) $|\tilde{I}(z)|$ for a lossless transmission line of characteristic impedance $Z_0=50$, terminated in a load with a reflection coefficient $\Gamma = 0.3e^{j30^\circ}$.The magnitude of the incident wave $|V_0^+| = 1$ V. The standing-wave ratio is

$$S = |\tilde{V}|_{\max}/|\tilde{V}|_{\min} \\ = 1.3/0.7 = 1.86$$



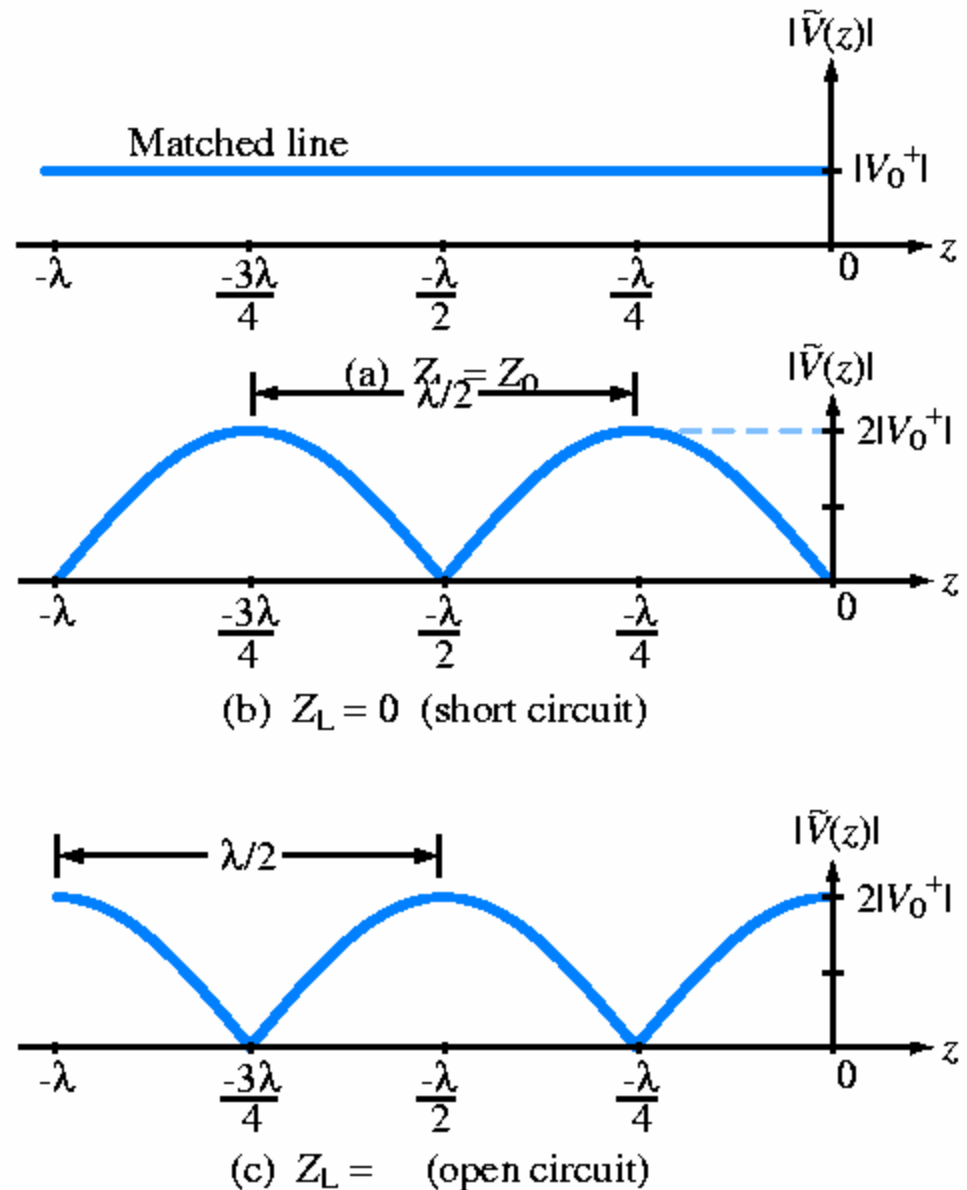
(a) $|\tilde{V}(z)|$ versus z



(b) $|\tilde{I}(z)|$ versus z

- sinusoidal pattern - standing wave caused by the interference of the two waves
- Matched line, $Z_L = Z_0$ with $|\Gamma| = 0$ and $|V(z)| = |V_0^+|$ for all values of $z \rightarrow$ with no reflected wave present, there will be no interference and no standing wave
- $|\Gamma| = 1$ and max of $|V(z)| = 2|V_0^+|$ and min of $|V(z)| = 0$
 - Short circuit, where $\Gamma = -1$
 - Open circuit, where $\Gamma = 1$

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- How to find the *max* & *min* position value of the voltage magnitude??

First voltage maximum

$$l_{\max} = -z$$
$$= \frac{\theta_r + 2n\pi}{2\beta} = \frac{\theta_r \lambda}{4\pi} + \frac{n\lambda}{2},$$
$$\begin{cases} n = 1, 2, \dots & \text{if } \theta_r < 0 \\ n = 0, 1, 2, \dots & \text{if } \theta_r \geq 0 \end{cases}$$

First voltage minimum

$$l_{\min} = \begin{cases} l_{\max} + \lambda/4, & \text{if } l_{\max} < \lambda/4 \\ l_{\max} - \lambda/4, & \text{if } l_{\max} \geq \lambda/4 \end{cases}$$

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- The ratio of $|\tilde{V}|_{\max}$ to $|\tilde{V}|_{\min}$ is called *the voltage standing-wave ratio, S or VSWR* and is given by

$$S = \frac{|\tilde{V}|_{\max}}{|\tilde{V}|_{\min}} = \frac{1 + |\Gamma|}{1 - |\Gamma|} \text{ (dimensionless)}$$

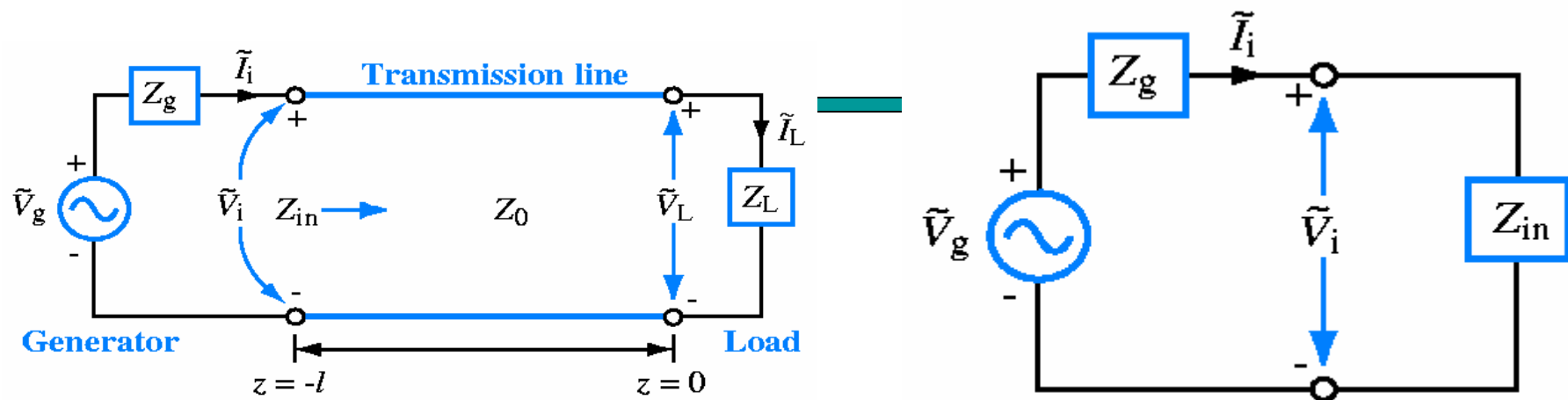
- For a **matched load** : $\Gamma = 0, \therefore S = 1$
- For a **line** : $|\Gamma| = 1, \therefore S = \infty$

Exercise 5

A 50Ω transmission line is terminated in a load with $Z_L = (100 + j50)\Omega$. Find the voltage reflection coefficient and the voltage standing wave ratio (VSWR).

7.6 Input impedance of lossless line

- the standing wave pattern indicate that for a mismatched line the voltage and current magnitudes are oscillatory with position on the line and in phase opposition with each other.
- Hence, the voltage to current ratio Z_{in} , must vary with position
- Z_{in} is define as '*the ratio of the total voltage (incident & reflected wave) to the total current at any point z on the line.*'



$$Z_{in}(-l) = Z_0 \left(\frac{Z_L \cos \beta l + jZ_0 \sin \beta l}{Z_0 \cos \beta l + jZ_L \sin \beta l} \right)$$

$$= Z_0 \left(\frac{Z_L + jZ_0 \tan \beta l}{Z_0 + jZ_L \tan \beta l} \right)$$

Voltage amp of incident wave

$$V_0^+ = \left(\frac{V_g Z_{in}}{Z_g + Z_{in}} \right) \left(\frac{1}{e^{j\beta l} + \Gamma e^{-j\beta l}} \right)$$

Exercise 6

A 1.05 GHz generator circuit with series impedance $Z_g = 10\Omega$ and voltage source given by

$$v_g(t) = 10\sin(\omega t + 30^\circ)$$

Is connected to a load $Z_L = (100 + j50)\Omega$ through a 50Ω , 67cm long lossless transmission line. The phase velocity of the line is $0.7c$, c is the velocity of light in a vacuum. Find

- a) λ
- b) β
- c) Γ
- d) Z_{in}

**GOOD LUCK for FINAL PAPER
&
All the best !!**

Thank you