

### Solution of Sheet # 3 (Shaft Design)

**Example 1** A line shaft supporting two pulleys A and B is shown in Fig. 9.2 (a). Power is supplied to the shaft by means of a vertical belt on pulley A, which is then transmitted to pulley B carrying a horizontal belt. The ratio of belt tensions on tight and loose sides is 3 : 1 and the maximum tension in either belt is limited to 2.7 kN. The shaft is made of plain carbon steel 40C8 ( $S_{ut} = 650 \text{ N/mm}^2$  and  $S_{yt} = 380 \text{ N/mm}^2$ ). The pulleys are keyed to the shaft. Determine the shaft diameter according to the A.S.M.E. code if

$$k_b = 1.5 \quad \text{and} \quad k_t = 1.0$$

**Solution**  $0.30S_{yt} = (0.30)(380) = 114 \text{ N/mm}^2$

$$0.18S_{ut} = (0.18)(650) = 117 \text{ N/mm}^2$$

The lower of the two values is  $114 \text{ N/mm}^2$  and there are keyways on shaft. Therefore

$$\tau_d = (0.75)(114) = 85.5 \text{ N/mm}^2 \quad (i)$$

The maximum belt tension will occur in belt on pulley A due to smaller diameter. The tensions on the tight and loose sides of this belt are 2700 N and 900 N, respectively.

The torque supplied to the shaft is given by

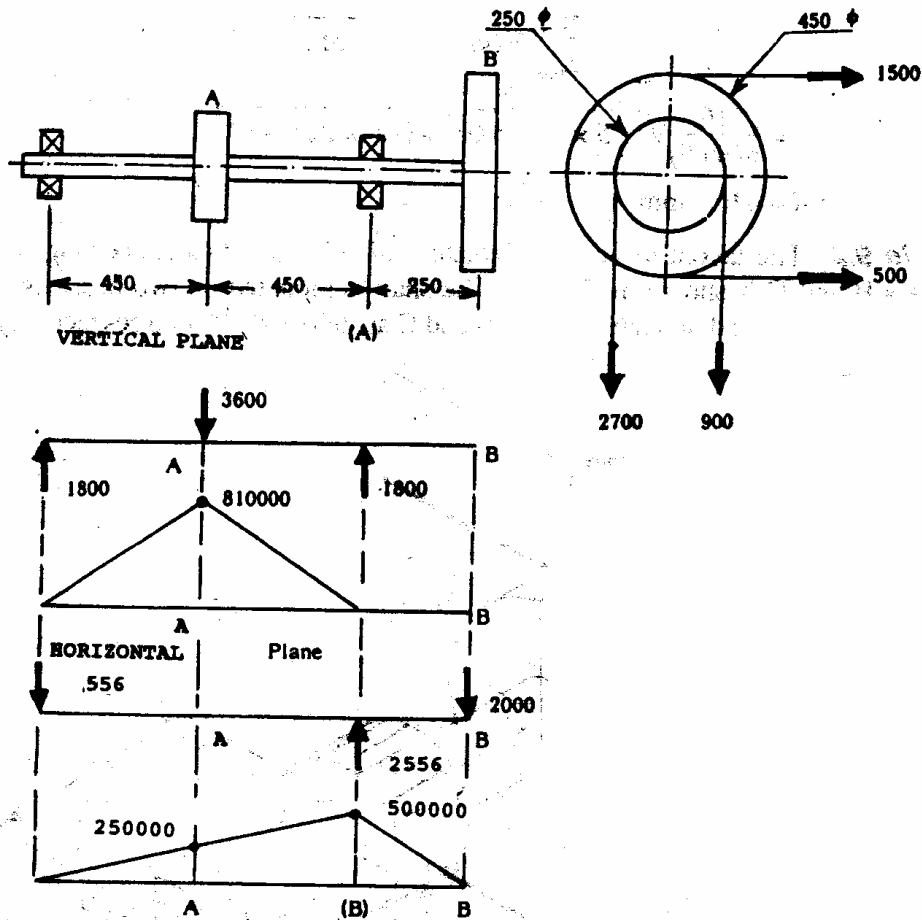


Fig. 9.2

$$M_t = (2700 - 900) \left( \frac{250}{2} \right) = 225\,000 \text{ N-mm}$$

The belt tensions for pulley B are  $P_{B1}$  and  $P_{B2}$ . Therefore,

$$\frac{P_{B1}}{P_{B2}} = 3 \quad (a)$$

and  $(P_{B1} - P_{B2}) \left( \frac{450}{2} \right) = 225\,000 \quad (b)$

Solving Eqs (a) and (b),

$$P_{B1} = 1500 \text{ N} \quad \text{and} \quad P_{B2} = 500 \text{ N}$$

The forces and bending moments in vertical and horizontal planes are shown in Fig. 9.2 (b). The maximum bending moment is at A. The resultant bending moment is given by

$$M_b = \sqrt{(810\,000)^2 + (225\,000)^2} = 847\,703 \text{ N-mm}$$

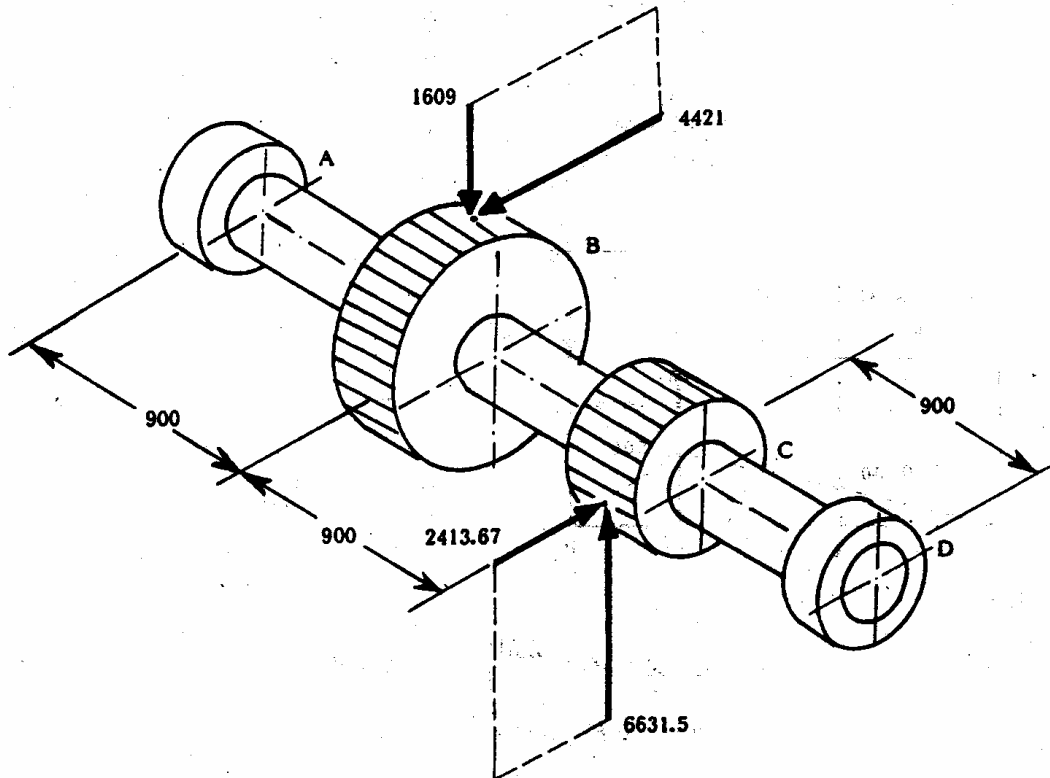
From Eq. (9.4),

$$d^3 = \frac{16}{\pi \tau_{\max}} \sqrt{(k_b M_b)^2 + (k_t M_t)^2}$$

$$= \frac{16}{\pi (85.5)} \sqrt{(1.5 \times 847\,703)^2 + (1.0 \times 225\,000)^2}$$

$$\therefore d = 42.53 \text{ mm}$$

**Example 2** The layout of an intermediate shaft of a gear box supporting two spur gears B and C is shown in Fig. 9.3. The shaft is mounted on two bearings A and D. The pitch circle diameters of gears B and C are 900 and 600 mm respectively.



The material of the shaft is steel ( $S_{ut} = 770$  and  $S_{yt} = 580 \text{ N/mm}^2$ ). The factors  $k_b$  and  $k_t$  of A.S.M.E. code are 1.5 and 2.0 respectively. Determine the shaft diameter using the A.S.M.E. code.

Assume that the gears are keyed to the shaft.

**Solution**  $0.30S_{yt} = 0.30(580) = 174 \text{ N/mm}^2$

$$0.18S_{ut} = 0.18(770) = 138.6 \text{ N/mm}^2$$

Since the gears are keyed to the shaft, therefore,

$$\tau_{\max} = 0.75(138.6) = 103.95 \text{ N/mm}^2$$

The forces and bending moments in vertical and horizontal planes are shown in Fig. 9.4. The resultant bending moment is maximum at C.

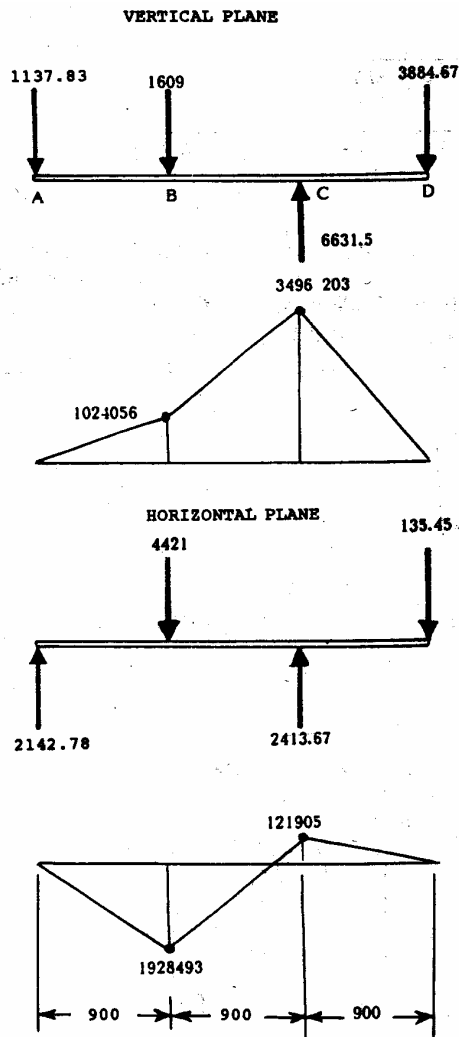


Fig. 9.4

At C,

$$M_b = \sqrt{(3496203)^2 + (121905)^2}$$

$$= 3498327.4 \text{ N-mm}$$

and

$$M_t = (4421)(450)$$

$$= 1989450 \text{ N-mm}$$

From Eq. (9.4)

$$d^3 = \frac{16}{\pi \tau_{\max}} \sqrt{(k_b M_b)^2 + (k_t M_t)^2}$$

$$= \frac{16}{\pi (103.95)} \sqrt{(1.5 \times 3498327.4)^2 + (2 \times 1989450)^2}$$

$$\therefore d = 68.59 \text{ mm}$$