

DRAIN CURRENT MODEL

The channel under the gate oxide can be divided into two regions . In the linear region , lateral electric field is negligible . and the other , saturation region where the 2D effects are serious and lateral field cannot be neglected . The two regions are modelled separately .

The Linear Region

The current model is based on the hydrodynamic model .

From the previous chapter ,

$$\mu = \mu_0 \frac{1}{1 + \beta E y \exp \frac{-y}{L_v} + \alpha E (1 - \exp \frac{-y}{L_v})}$$

mobility is phenomenologically expressed as :

In the channel region ,

Free surface charge density $Q(y)$ is given as

$$Q(y) = -C_{ox} [V_{gs} - (V_t - \Delta V_t) - (1 + \delta)V(y)]$$

where $V(y)$ is the channel potential and δ is explained later .

The Current is given as

$$I_{ds} = Q(y) \mu_n(y) E_y$$

$$I_{ds} = C_{ox} [V_{gs} - (V_t - \Delta V_t) - V(y)] \mu_n(y) \frac{\partial V}{\partial y}$$

Putting the expression for mobility ,

$$I_{ds} = C_{ox} [V_{gs} - (V_t - \Delta V_t) - V(y)] \mu_n^0 \frac{\partial V}{\partial y} \frac{1}{1 + \beta E_y y \exp\left(\frac{-y}{L_v}\right) + \alpha E_y (1 - \exp\left(\frac{-y}{L_v}\right))}$$

Bringing denominator of RHS to LHS and multiplying with current gives,

$$\begin{aligned} & \int_0^L I_{ds} \left[1 + \beta E_y y \exp\left(\frac{-y}{L_v}\right) + \alpha \frac{\partial V}{\partial y} + \alpha \exp\left(\frac{-y}{L_v}\right) \right] dy \\ &= I_{ds} \left[L + \alpha \int_0^{V_{ds}} dV + \int_0^L \left[\beta E_y y \exp\left(\frac{-y}{L_v}\right) + \alpha E_y \exp\left(\frac{-y}{L_v}\right) \right] dy \right] \end{aligned}$$

Approximately the expression becomes by assuming electric field to be constant and equal to the electric field as source end,

$$\begin{aligned} &= I_{ds} \left[L + V_{ds} + E(0) \int_0^L \beta y \exp\left(\frac{-y}{L_v}\right) dy - E(0) \int_0^L \alpha \exp\left(\frac{-y}{L_v}\right) dy \right] \\ &= I_{ds} \left[L + V_{ds} + \alpha E(0) L_v \left\{ \exp\left(\frac{-L}{L_v}\right) - 1 \right\} + \beta E(0) \left\{ L^2_v - L L_v \exp\left(\frac{-L}{L_v}\right) - L^2_v \exp\left(\frac{-L}{L_v}\right) \right\} \right] \end{aligned}$$

$$= I_{ds} [L + V_{ds} - \alpha E(0)L_v + \beta E(0)L_v^2]$$

Carrying out the RHS integral and equating with LHS ,

$$I_{ds} = \frac{W \mu_n^0 C_{ox} \{V_{gst} V_{ds} - \frac{(1 + \delta)V_{ds}^2}{2}\}}{L + \alpha V_{ds} + E_y(0) \{ \beta L_v^2 - \alpha L_v \}}$$

To calculate the electric field at source end we note that,

at $y=0$

$$I_{ds} = WC_{ox} \mu_n^0 [V_{gs} - V_t + \Delta V_t] E_y(0)$$

Also from previous equation, current may be calculated as ,

$$I_{ds} = \frac{W \mu_n^0 C_{ox} \{V_{gst} V_{ds} - \frac{(1 + \delta)V_{ds}^2}{2}\}}{L + \alpha V_{ds} + E_y(0) \{ \beta L_v^2 - \alpha L_v \}}$$

Which by inserting the expression for $E_y(0)$ reduces to ,

$$I_{ds} = \frac{W \mu_n^0 C_{ox} \{V_{gst} V_{ds} - \frac{(1 + \delta)V_{ds}^2}{2}\}}{L + \alpha V_{ds} + \{ \beta L_v^2 - \alpha L_v \} \frac{I_{ds}}{WC_{ox} \mu_n^0 [V_{gs} - V_t + \Delta V_t]}}$$

We may write the expression for drain current as,

$$I_{ds} = \frac{-A_2 + \sqrt{A_2^2 - 4A_1A_3}}{2A_1}$$

$$A_1 = \frac{\{\beta L^2 v - \alpha L v\}}{W\mu_n^0 C_{ox} V_{gst}}$$

$$A_2 = L + \alpha V_{ds}$$

$$A_3 = -W\mu_n^0 C_{ox} [V_{gst} V_{ds} - \frac{(1 + \delta)V_{ds}^2}{2}]$$
