

TRANSPORT AND MOBILITY MODEL FOR SMALL DEVICES

For small devices of sub-micron channel lengths, the drift-diffusion model is not very accurate . The drift-diffusion (DD) model assumes small perturbations around equilibrium . For channel lengths less than 0.25 μm the perturbation from equilibrium is large due to the presence of large lateral field and their gradients.

Device Simulator like PISCES employs a local-field model to find the current generation in short channel devices . This type of model assumes that the carrier acquires the steady-state energy corresponding to the local field at each grid point .

In small devices, the mobile carriers do not have enough time to reach equilibrium . With the increased applied electric field ,the velocity overshoot effect becomes apparent . This effects the energy distribution of the electron and the electron energy can depart from its value in thermal equilibrium .

One of the ways to incorporate the above effects is to base a model based on electron transport at microscopic level . But it is too time consuming and therefore inappropriate for device simulators.

The Hydrodynamic Model

The energy transport equation is based on Hydrodynamic Model . This model incorporates electron temperature and energy flux in the device .

The hydrodynamic equations are given as :

$$\frac{\partial n}{\partial t} + \nabla \cdot (nv) = \frac{dn}{dt}$$

$$\frac{\partial v}{\partial t} + (v \cdot \nabla)v = \frac{eE}{m^*} - \frac{n \nabla(nkT)}{m^*} + \frac{dv}{dt}$$

$$\frac{\partial w}{\partial t} + v \cdot \nabla w = ev \cdot E - \frac{\nabla(nvkT)}{n} + \frac{dw}{dt}$$

where

- n : carrier concentration
- e : electronic charge
- v : drift velocity
- w : average carrier energy
- E : electric field

Certain Assumptions are made for solving the equations :

- 1) Steady State (which eliminates time derivatives)
- 2) Very small kinetic energy so that average electron energy can be approximated as thermal energy ($w=1.5kT$)

Then the equations become :

$$\frac{\partial n}{\partial t} + \nabla \cdot (nv) = 0$$

$$v = \frac{\tau}{m^*} \left[eE - \frac{2 \nabla w}{3} - \frac{2}{3n} w \nabla n \right] + \frac{2\tau \nabla(v^2/2)}{3}$$

and τ is energy relaxation time .

Equation (2) can be written as :

$$\frac{\partial w}{\partial t} + v \cdot \nabla w = ev \cdot E_y - \frac{\nabla(nvkT)}{n} + \frac{(w_n - w_0)}{\tau}$$

The carrier energy density is,

$$W_n = n \cdot w_n$$

Therefore the above equation can be written as :

$$n \cdot \frac{\partial w}{\partial t} + nv \cdot \nabla w = envE_y - n \frac{\nabla(nvkT)}{n} + n \cdot \frac{(w_n - w_0)}{\tau}$$

Or,

$$\frac{\partial W_n}{\partial t} = -\nabla(nvw + nvkT) + \frac{(W_n - W_0)}{\tau} - envE_y$$

where carrier energy density in thermal equilibrium

$$W_0 = \frac{3nkT_0}{2}$$

The Energy Relaxation Time is empirically expressed as:

$$\tau = \frac{3kT\mu_n}{2qv_{sat}}$$

When the MOS device is operating in strong inversion Region , the carrier velocity can be expressed as :
(neglecting the diffusion current)

$$v = \mu_n \left(\frac{\partial \psi}{\partial y} - \frac{\partial U_n}{\partial y} \right)$$

where U is the thermal voltage of the carriers

$$\text{i.e. } U = \frac{kT}{q}$$

$$\text{Therefore } W = \frac{3nkT}{2} = \frac{3n.q.U}{2}$$

$$\text{At steady state, } \frac{\partial W}{\partial t} = 0$$

That is,

$$0 = \frac{-\partial}{\partial y} \left[\left\{ \frac{3nqU}{2} + nqU \right\} \mu_n \left\{ \frac{\partial \psi}{\partial y} - \frac{\partial U}{\partial y} \right\} \right] \\ - \mu_n q n \left[\frac{\partial \psi}{\partial y} - \frac{\partial U}{\partial y} \right] \cdot \frac{\partial \psi}{\partial y} - \frac{(W_n - W_0)}{\tau}$$

Or,

$$-\frac{7nq\mu}{2} \cdot \frac{\partial U}{\partial y} \cdot \frac{\partial \psi}{\partial y} + \frac{5nq\mu}{2} \cdot \left(\frac{\partial U}{\partial y} \right)^2 + nq\mu \cdot \left(\frac{\partial \psi}{\partial y} \right)^2 \\ = \frac{nq(U - U_0)}{2\tau}$$

This equation will be used further when we develop the Mobility Model .

MOBILITY MODEL

Starting with the equation (From the Hydrodynamic model)

$$\frac{-7}{2} \left(\frac{\partial U}{\partial y} \right) \left(\frac{\partial \psi}{\partial y} \right) + \frac{5}{2} \left(\frac{\partial U}{\partial y} \right)^2 + \left(\frac{\partial \psi}{\partial y} \right)^2 = \frac{3(U_n - U_0)}{2\tau_e \mu^0}$$

We also assume the **non-local** mobility equation as :

$$\mu_n = \mu^0 \frac{T_0}{T} = \mu^0 \frac{U_0}{U_n}$$

We use the following approximation ,

$$\frac{\partial U}{\partial y} = \frac{(U - U_0)}{y}$$

The above equation can thus be written as

$$\frac{-7}{2} \left(\frac{U_n - U_0}{y} \right) E_y + \frac{5}{2} \left(\frac{U_n - U_0}{y} \right)^2 + E_y^2 = \frac{3(U_n - U_0)}{2\tau_e \mu^0}$$

Or,

$$\left\{ \frac{5}{2} - \frac{3y^2}{2\tau_e \mu_0} \right\} U_n^2 + U_n \left\{ \frac{7}{2} y E_y + \frac{3y}{2\tau_e \mu_0} \right\} + E_y^2 = 0$$

(where E is the magnitude of electric field)

From the equation , U can be expressed as

$$U_n = U_0 + \frac{A_2 - \sqrt{A_2^2 - 4A_1 A_3}}{2A_1}$$

Where

$$A_1 = \frac{5}{2} - 3 \frac{y^2}{2\tau_e \mu_0 U_0}$$

$$A_3 = E_y^2$$

$$A_2 = \frac{-7}{2} E_y + 3 \frac{y}{2\tau_e \mu_0}$$

Approximate expression for mobility

Let us define a parameter as $L_v = \frac{7\tau_e\mu_0 E_y}{3}$

Within the device y varies from 0 to L .

- 1) For $y \gg L_v$ the expression can be further approximated as (See Appendix B)

$$U = U_0 \cdot \left[\frac{1 + \sqrt{1 + \frac{8\tau\mu_0 E_y^2}{3}}}{2} \right]$$

Or,

$$\frac{\mu_0}{\mu_n} = \left[\frac{1 + \sqrt{1 + \frac{8\tau\mu_0 E_y^2}{3}}}{2} \right]$$

Or,

$$\mu_n = \mu_0 \cdot \left[\frac{2}{1 + \sqrt{1 + \frac{8\tau\mu_0 E_y^2}{3}}} \right]$$

Or,

$$\mu_n = \mu_0 \cdot \left[\frac{1}{1 + \alpha E_y} \right]$$

Where α is defined to be

$$\alpha = \frac{-1 + \sqrt{1 + \frac{8\tau\mu_n^0 E_y^2}{3U_l}}}{2E_y}$$

The significance of this parameter will be explained later

2) For $y < L_v$, the mobility expression can be found by approximating,

$$A_1 = \frac{5}{2} \quad A_2 = \frac{7}{2} \quad A_3 = E_y^2$$

The expression for U becomes as

$$U_n = U_0 + y \cdot \frac{\frac{7E_y}{2} - \sqrt{\frac{49E_y^2}{4} - 10E_y^2}}{5}$$

Or,

$$U_n = U_0 + y \cdot \frac{\frac{7E_y}{2} - \frac{3E_y}{2}}{5} = U_0 + \frac{2U_0}{5U_0} \cdot y \cdot E_y$$

Or,

$$\mu = \mu_0 \frac{1}{1 + \beta y E_y} \quad \text{where } \beta = \frac{2}{5U_0}$$

The second step to finding an approximate expression for Mobility is phenomenological

$$\mu = \frac{\mu_0}{1 + \beta \cdot y \cdot E_y \cdot \exp\left(\frac{-y}{L_v}\right) + \alpha \cdot E_y \cdot \{1 - \exp\left(\frac{-y}{L_v}\right)\}}$$

The Denominator D is $1 + \beta \cdot y \cdot E_y$ for small y

and for y large $1 + \alpha \cdot E_y \cdot \{1 - 0\} = 1 + \alpha \cdot E_y$

Fig 1 : Mobility Curve for L=0.67 microns for constant electric field

Fig 2 : Electric field variation along the MOSFET channel for different drain voltages

