

Chapter: **AFX 'V'ariable**



this is the Best-of-AFX Phase-Filter Circuit Design

Non-Resonant Dual-Notch Phase-Filter-

******* Goals achieved in AFX-'V' :**

- *** (1) Simpler design,**
- *** (2) Simpler construction,**
- *** (3) Simpler adjustment.**
- *** (4) Enhanced Variability $f(0)$**

Continued Design features from AFX:

***** Improved design from building-block modules**

**3 Filters are $Q=3$, 1 Filter $Q=5$,
all $R(\text{freq})$ aprox. Same.**

Enables use of single control of four $R(\text{freq})$ stages.

***** Designed so that the High 'Q' Sharp Filter is also variable
within the main band-pass.**

***** Designed so that the Dual-Notches
are < -60 dB and the Stop-Band < -100 dB .**

Design choices:

*** Simple repetitive application of Modified *Delyannis-Friend*-Multiple-FeedBack design.

*** MFB topology was chosen because :

- *** (1) input vs output impedances match well, loading is naturally controlled.
- *** (2) single resistor frequency control each stage.
- *** (3) frequency adjustments alters gain by only the square-root of the f(change) .

Just for reference:

Delyannis-Friend Multiple-Feed-Back design

MULTIPLE FEEDBACK BAND-PASS DESIGN EQUATIONS

$$\frac{-H \omega_0 s}{s^2 + \alpha \omega_0 s + \omega_0^2}$$

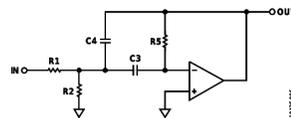


Figure 6.

$$\frac{V_o}{V_{in}} = \frac{-s \frac{1}{R_1 C_4}}{s^2 + s \frac{C_3 + C_4}{C_3 C_4 R_5} + \frac{1}{R_5 C_3 C_4} \left(\frac{1}{R_1} + \frac{1}{R_2} \right)}$$

To design the filter, choose C3.

Then

$$k = 2 \pi F_0 C_3$$

$$C_4 = C_3$$

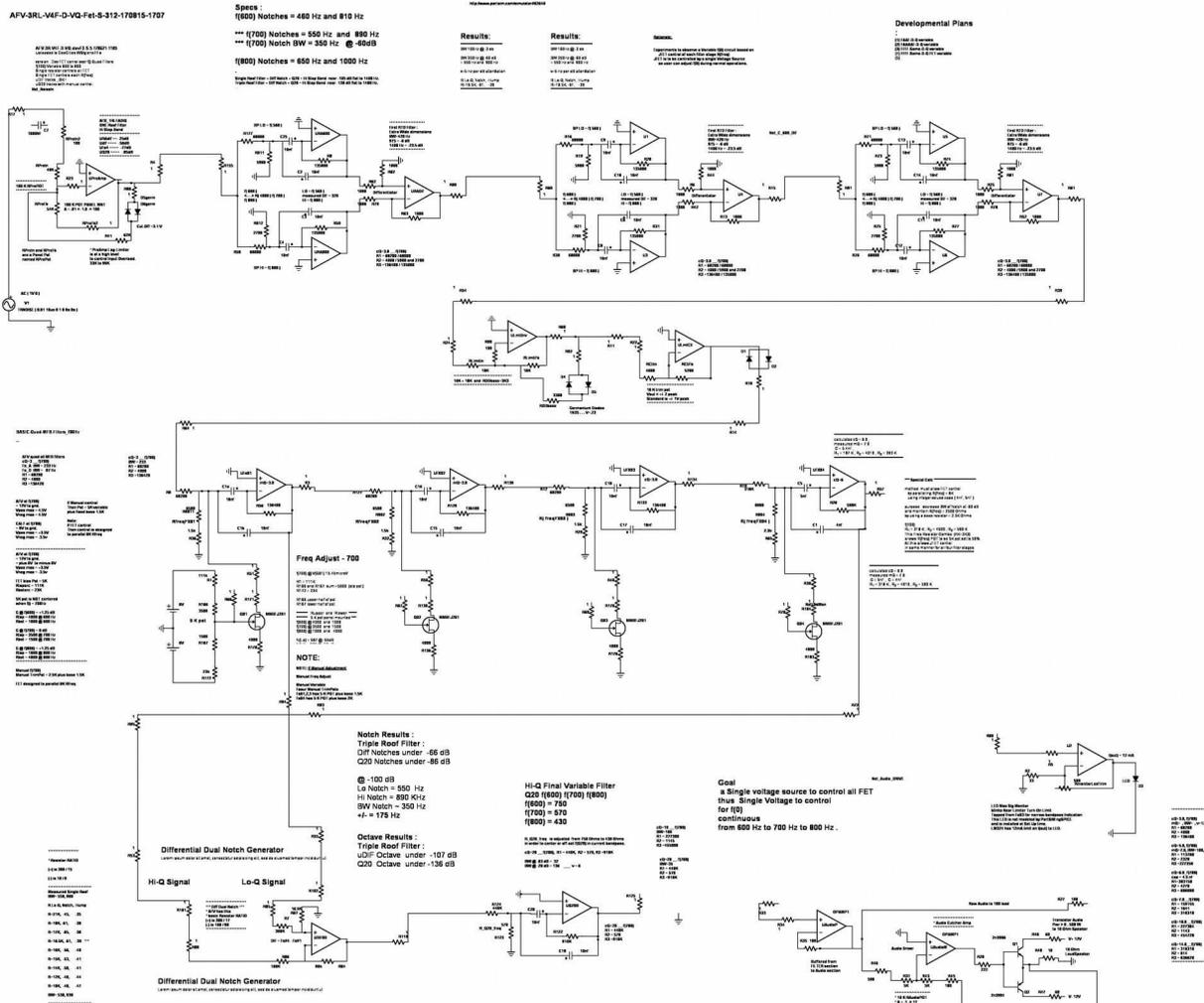
$$R_1 = \frac{1}{H k}$$

$$R_2 = \frac{1}{(2Q - H)k}$$

$$R_5 = \frac{2Q}{k}$$

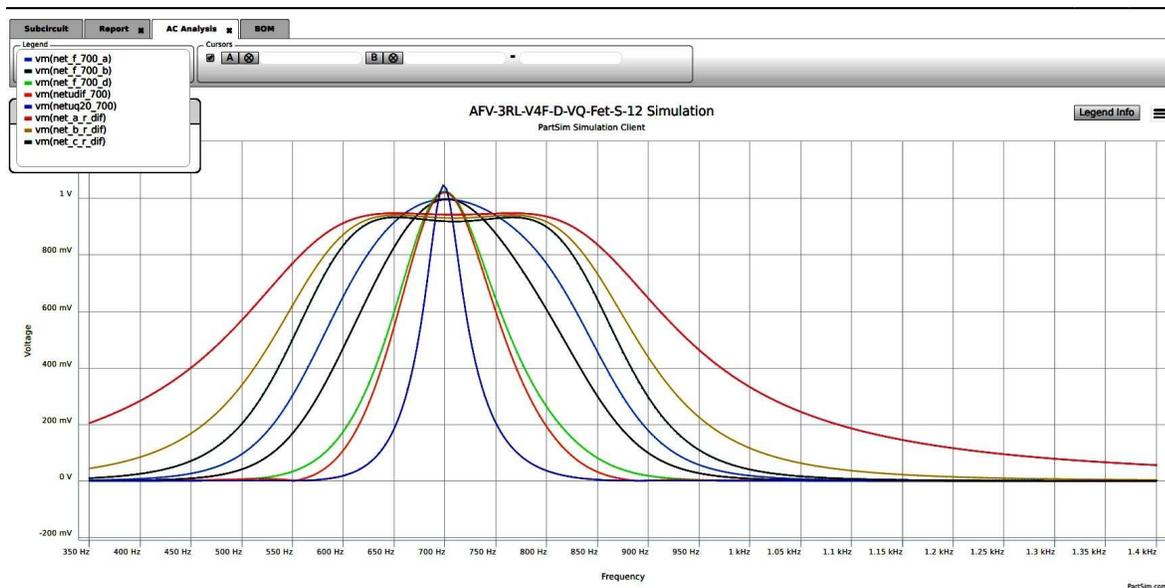
Delyannis-Friend Multiple-Feed-Back design

Circuit : "AFX-V-3RL-v4F-D-vQ-Fet"

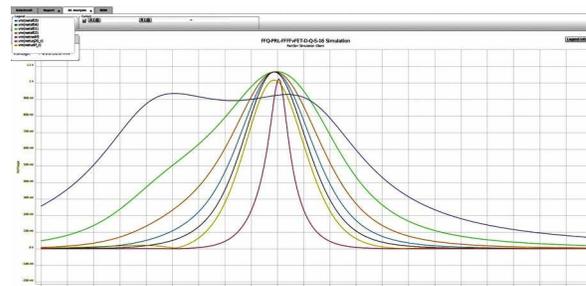
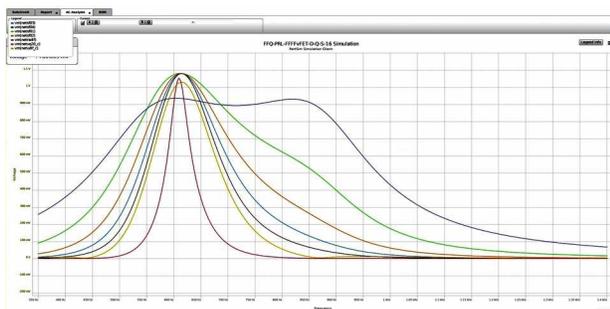


Bode Plot: **AFV-3RL-v4F-D-vQ-Fet**

Roofing Filter Output is (red), very wide which contains the variability of the central f() signal



****** Below : shown adjusted 600Hz , 700Hz , 800Hz**
******* Notice that the peak amplitudes of the final signals stay within 0.3 dB of the f(700) signal.**



f() signal

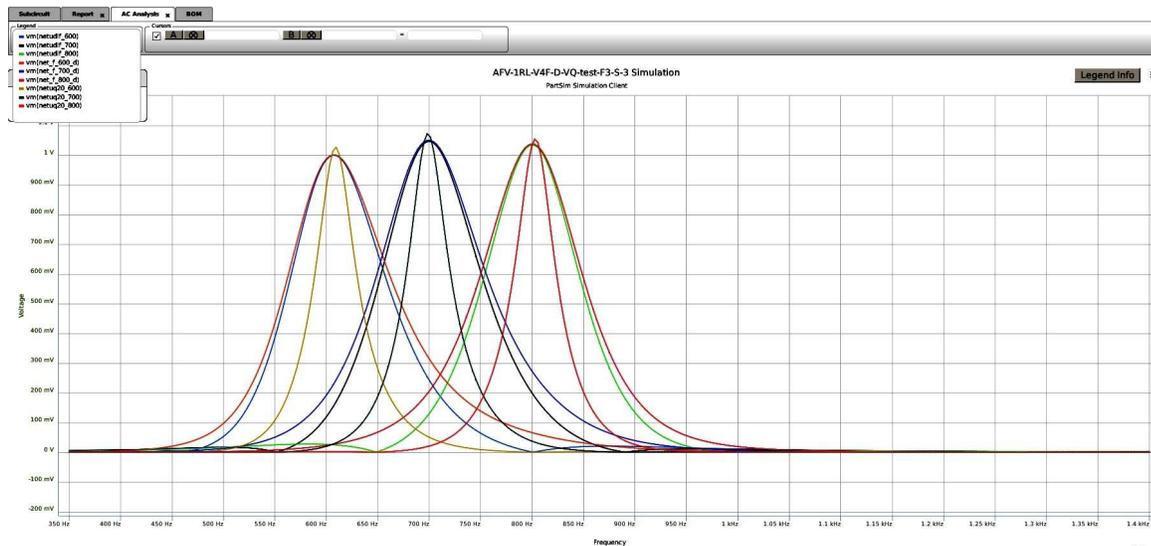
variability of the central

Notice that the 600 --- 800 waveforms have good central Band-Pass shapes.

Bode Plot: **advanced AFV circuit** utilizes
Three Triad-Roofing-Differential Filters for for max sideband control.

- *** **Dual-Notches are very Deep and Octave Stop-Band very low.**
- *** **Main Filter f(0) is Variable 600 - 700 - 800 by user in real-time.**
- *** **Sharp Q=20 filter is variable within the selected PassBand.**

- *** **Here, the R(freq) is currently controlled by one R(freq) Pot, which can be mounted on the front panel, for real-time control.**
- *** **The Four FET controllers are driven by a single Voltage Source, controlled by a Panel Mounted Pot.**
- *** **Front Panel Rotary Switch allows User to send any stage into the Audio Section.**
- *** **Front Panel Switch can be utilized to drive FxQ20 from any filter stage.**



Magnitude Plot: **AFV-3RL-v4F-D-vQ-Fet**



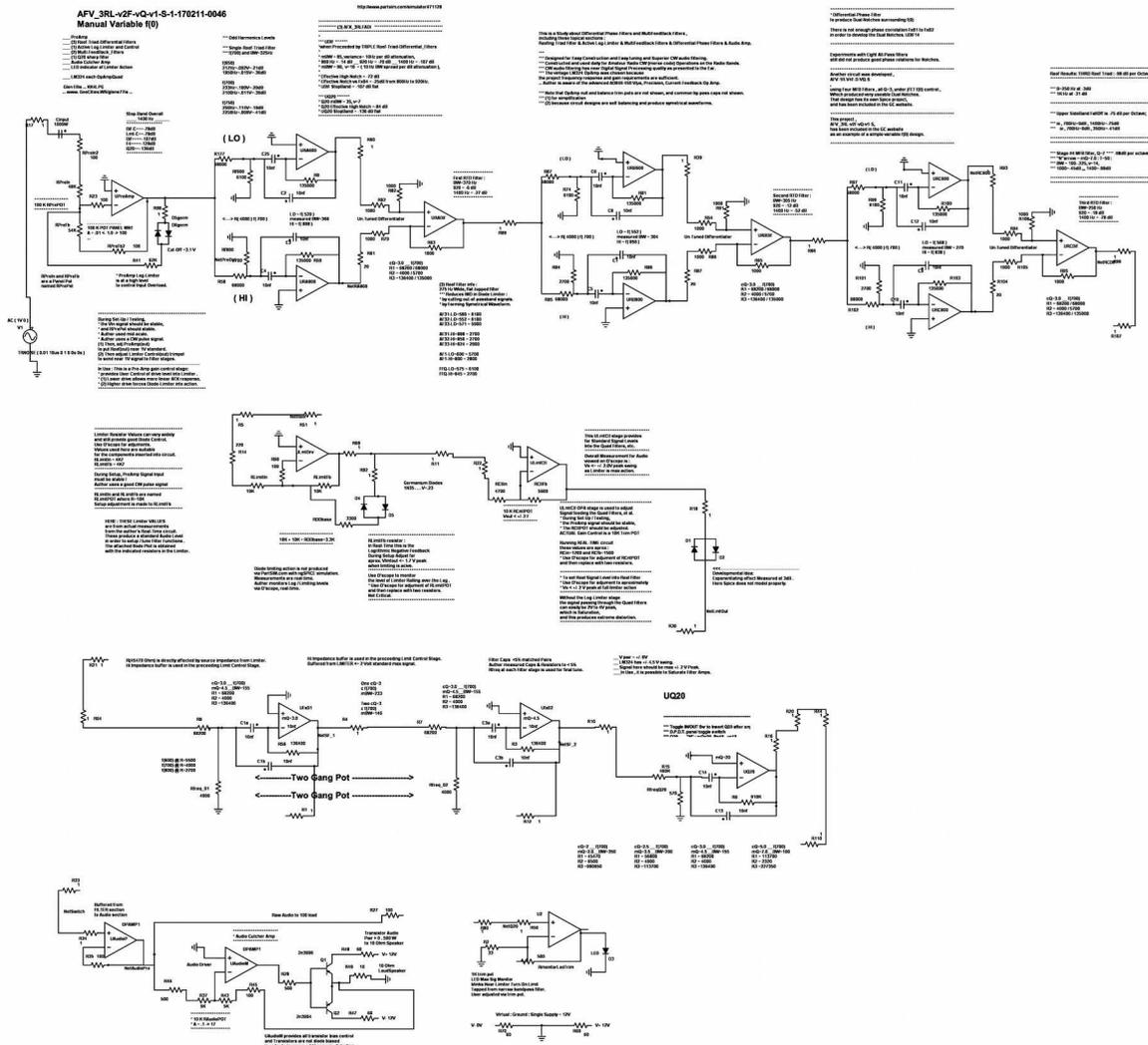
*** At 900 Hz, the **Red Dot on Notch** indicates **-86 dB attenuation** for the **f(700)** trace .
Trace to 1400 Hz is -76 dB attenuation.

circuit: **Sample: 'AFV_3RL-v2F-vQ-v1-S'**

This simple circuit was NOT spectacular but was given a fair test.

... Goal was to prove the use of only **Two MFB filters** which would require only a single dual-Pot for control of $f(0)$..

- *** AFV_3RL-v2F-vQ-v1-S design :
- *** (1) with **Three Roof Filters**
- *** (2) with only **Two MFB filter stages**
- *** (3) with R(freq) controlled by a **Two-Gang Pot**



Results: use of only **Two MFB filters**

which would require only a single dual-Pot for control of $f(0)$..

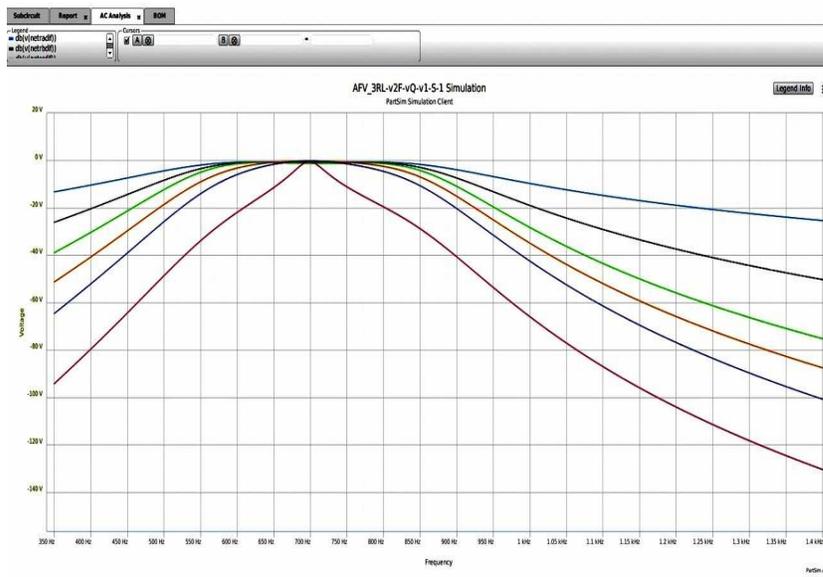
... Dual Notches could not be well developed when using only Two MFB filters.

... More Phase-Alignment in the filter module is required to generate the Dual Notches.

... Therefore,

No notches are presented in the below plots, and this is the best Bode Plot .

The Sharp Band-Pass comes from the two $Q=3$ final filters.







Chapter: **AFX_Filter_“T”**

Non-Resonant Dual-Notch Phase-Filter-

An AFX filter

Emphasizing the Roofing Filters “T” to supress the sidebands

- *** Triple Roof-Triad-Differential Filters preparing the signals**
- *** to drive a single Q=7 MFB bandpass filter**
- *** Triple Roof-Triad-Filter is 1400 Hz = -76 dB per octave.**
- *** Last stage Q=7 MFB is 1400 Hz = -98 dB per octave.**
- *** Last stage Q=20 MFB is 1400 Hz = -110 dB per octave.**

***** Roof-Triad-Filter info :**

***** all sections with same f(0) and same components .**

***** design is very tolerant of minor component variations .**

***** “cQ” is the calculated ‘Q’ for each stage :**

f(585) cQ=3.0 R(5800)

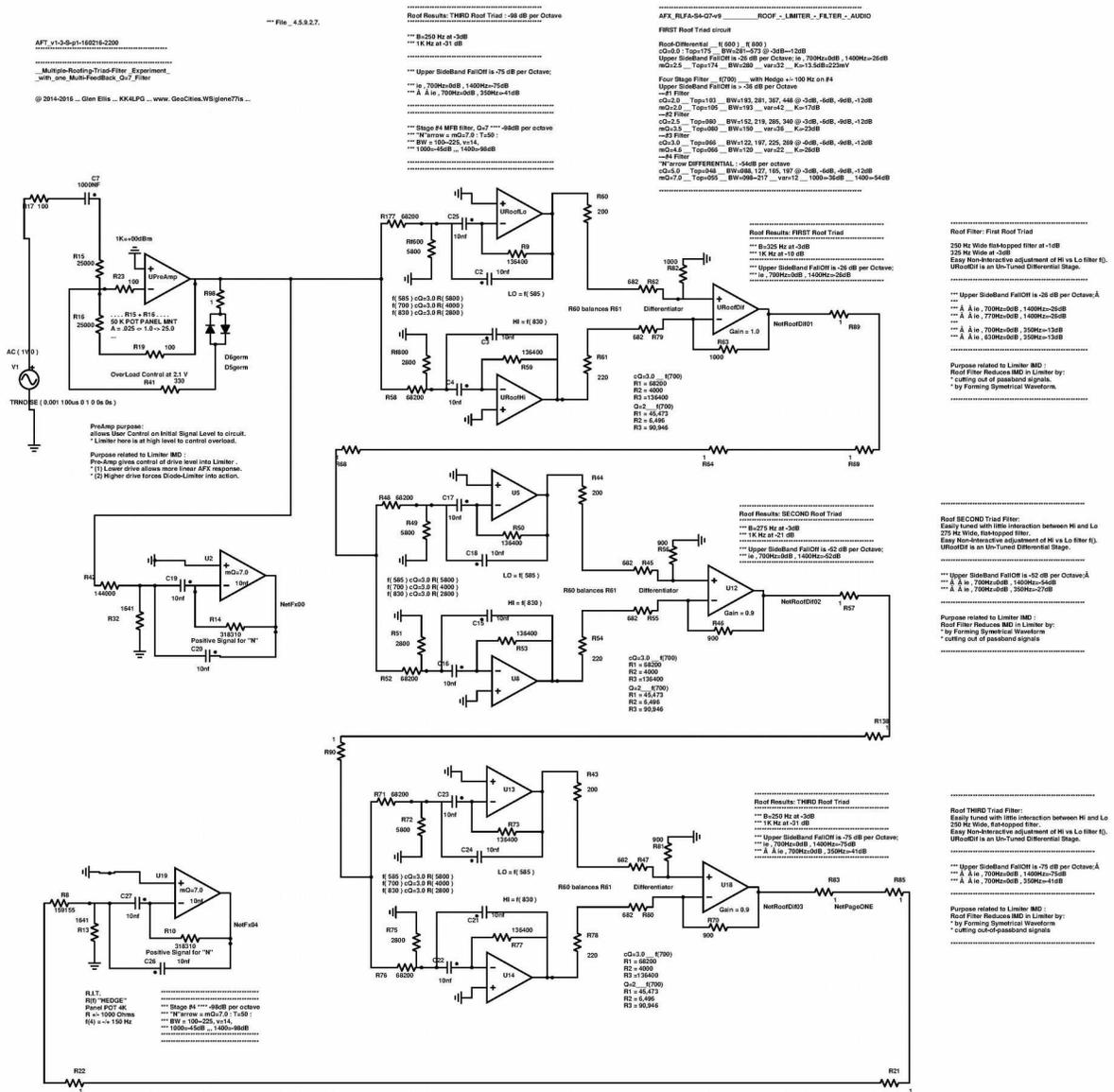
f(700) cQ=3.0 R(4000)

f(830) cQ=3.0 R(2800)

***** “mQ” is the measured ‘Q’ accumulated through to the last stage.**

Circuit: AFT_v1-3-S-p1

*** Triple Roof-Triad-Differential Filters plus one Q7 Filter.



Results: **AFT_v1-3-S-p1**

Roof Results: FIRST Roof Triad

calc design BW=325 Hz at -3dB
*** ie , 700Hz=0dB , 1400Hz=-26dB
*** ie , 700Hz=0dB , 350Hz=-13dB
*** SideBand Falloff is -26 dB per Octave;

Roof Results: SECOND Roof Triad

calc design BW=325 Hz at -3dB
*** ie , 700Hz=0dB , 1400Hz=-54dB
*** ie , 700Hz=0dB , 350Hz=-15dB
*** SideBand Falloff is -54 dB per Octave;

Roof Results: THIRD Roof Triad

calc design BW=325 Hz at -3dB
*** ie , 700Hz=0dB , 1400Hz=-75dB
*** ie , 700Hz=0dB , 350Hz=-18dB
*** SideBand Falloff is -75 dB per Octave;

*** Design for Sharp Filter *****

calc Design Final MFB filter, Q=7
*** BW = 100 @ -3 dB range=100---225, v=14,
*** 1000 Hz=-45dB ,, 1400 Hz = -98 dB

*** Cumulative Results after the Sharp Filter

*** cumulative measured results : Q=20
*** cumulative measured -98dB per octave
*** BW = 35 @ -3dB , range 35---126, v= 10,
*** 1000 Hz=-75dB ,, 1400 Hz = -110 dB

Chaper : AFX_pFilter_2_AFT ..210807... 4/7

Bode Plot: **AFT_v1-3-S-p1**

Triple Roof-Triad-Differential Filters plus one Q7 Filter. .

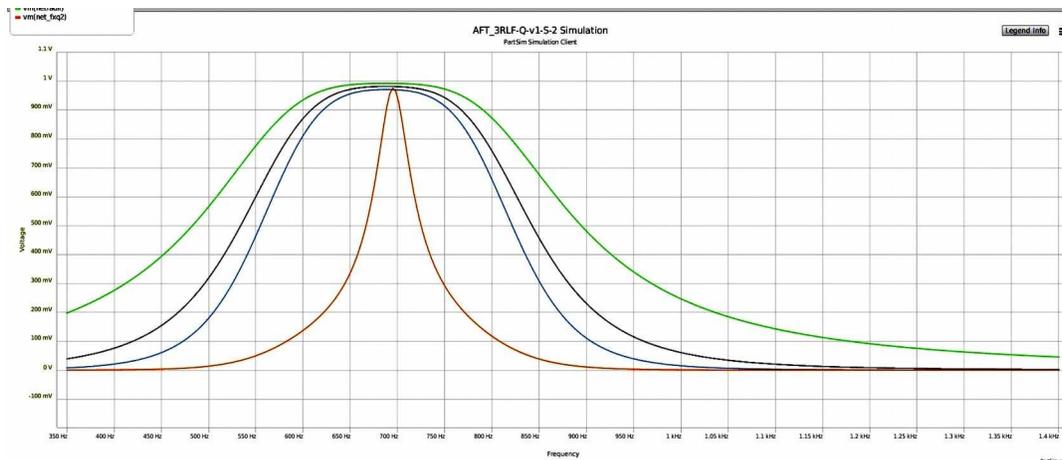
Most complex waveforms displayed.

Red trace is Q=7 signal **Before** Roofing Filters.

Yellow trace is Q=7 signal **After** Roofing Filters.



***** Notice the Roof Filters contribute to sideband suppression.**

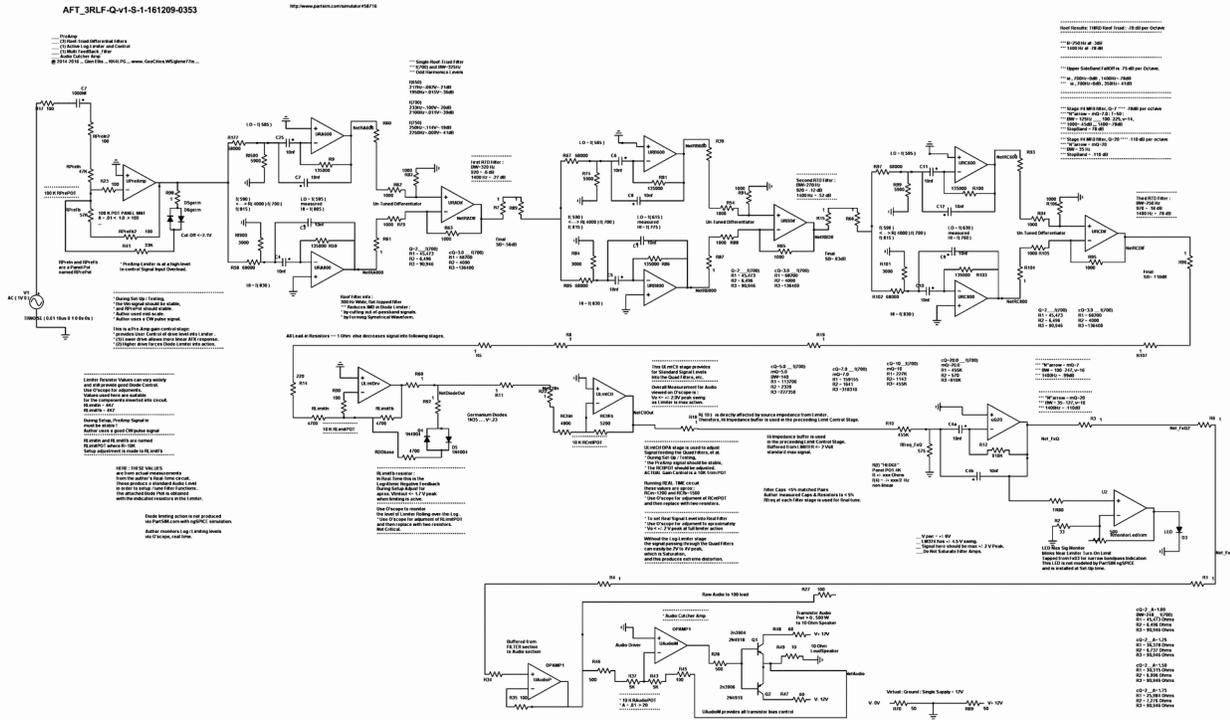


Circuit: **AFT_v1-3-S-p1**

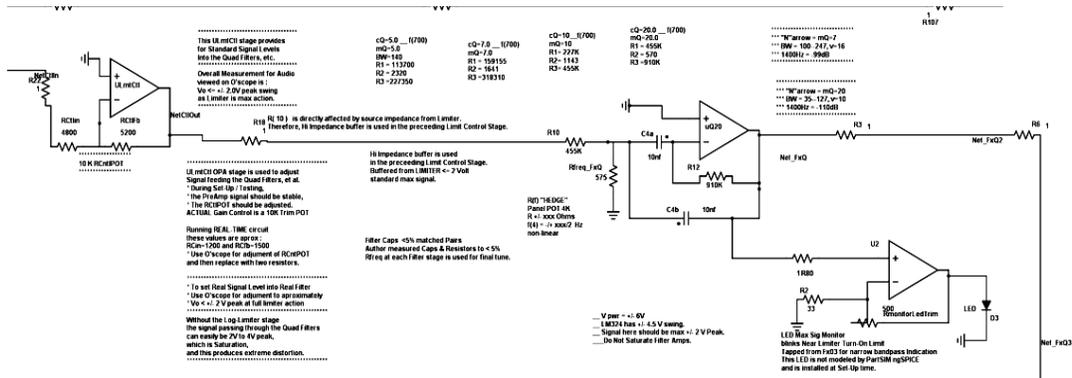
a Developed 'AFT' Circuit

*** No Dual Notches ***

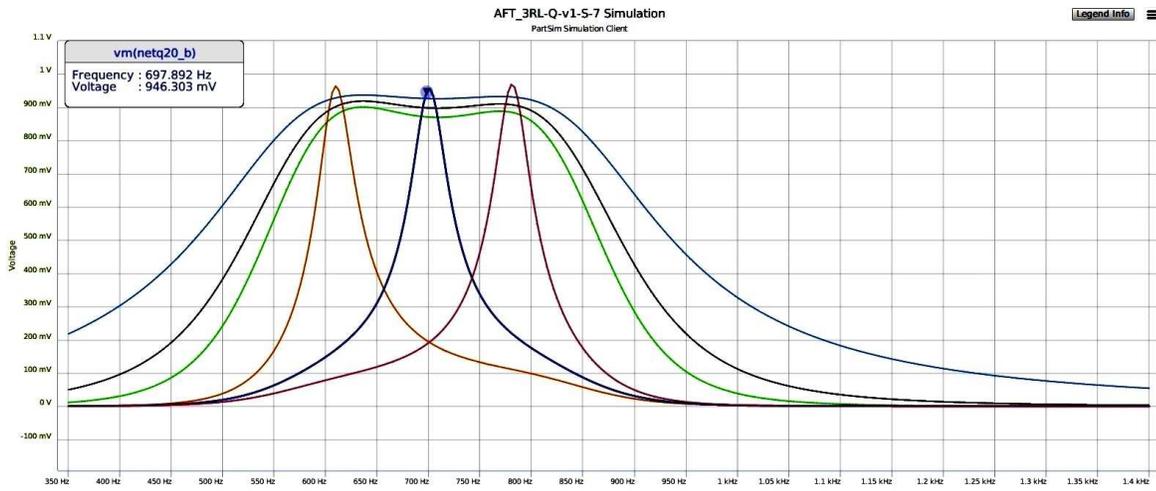
with PreAmp + three Roof-Filters + Active-Limiter + Q20 Filter + Audio :



Circuit: for single Narrow Filter:



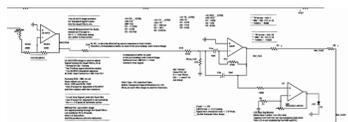
Bode Plot : **AFT_v1-3-S-p1**



f(0) adjusted 600 - 700-- 800

Chaper : AFX_pFilter_2_AFT ..210807... 7/7





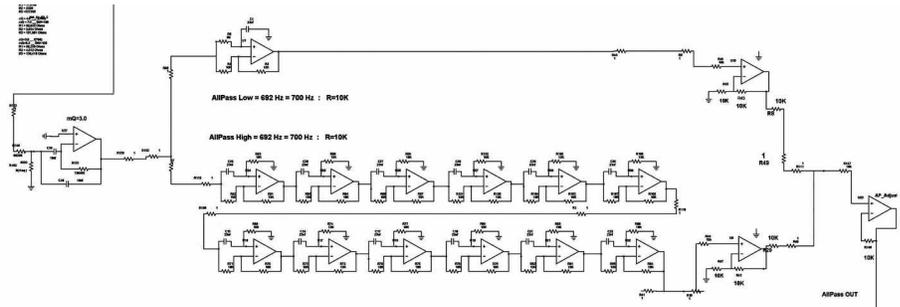
Chapter: All-Pass Band-Pass Filter



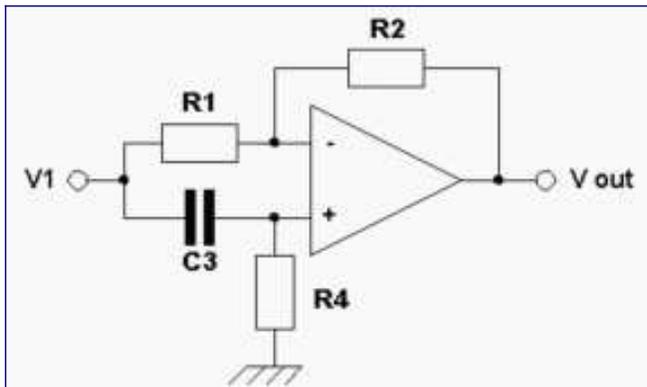
Phase-Filter Non-Resonant Dual-Notch

We examine a Phase-Filter-built from All-Pass Filters

Circuit: AFC core
1Lo-12Hi All-Pass

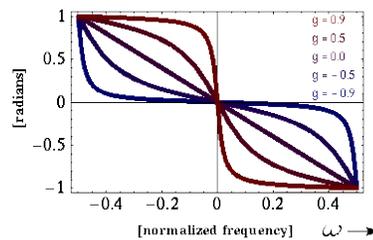


Some Electrical Theory
from common Electrical Engineering textbooks :



First-Order Allpass Phase Response (let $g = r e^{j\theta}$)

$$\Theta(\omega) \triangleq \angle H(e^{j\omega}) = -\omega - 2 \tan^{-1} \left[\frac{r \sin(\omega - \theta)}{1 - r \cos(\omega - \theta)} \right]$$



"The All-Pass filter has **frequency responses** which **must be zero at $w=0$ and at $w=\pi$.**" [wiki](#)

This paper presents

a **Non-Resonant Dual-Notch Phase-Filter**

producing a Band-Pass function

as an “ngSPICE project”

produced via the PartSIM.com browser based Simulator.

Introduction:

In all researched texts, the traditional academic texts specify

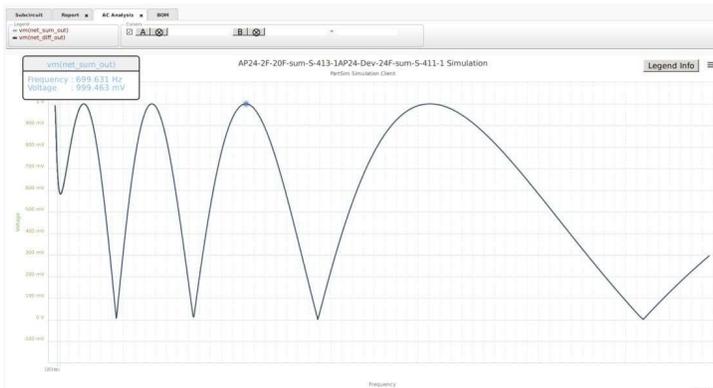
that **All-Pass** filters **CanNOT** be used

for **Low-Pass** nor **High-Pass** functions ,

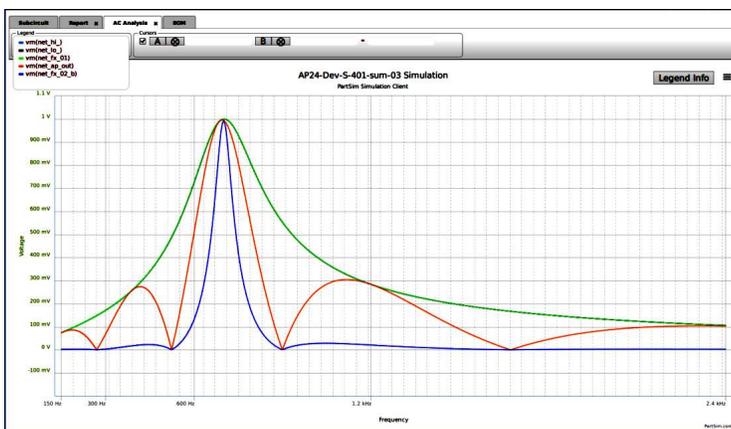
nor for **Band-Pass** functions.

*** However, the author has developed
working **Dual-Notch Band-Pass** circuits

*** which utilize the **All-Pass Filter**
in both LoPass and HiPass configurations



*** Raw All-Pass



*** Bode Plot
of “APC” circuit
All Vout signals

**In this #1 circuit,
f(Lo) = 700 Hz and f(Hi) = 700 Hz
This accentuated the "w" notches at :
each "0" point
each "pi" point
in the spectrum.**

***** In the #1 fully developed working circuit,
*** based on normal f(Lo) = 700 Hz and f(Hi) = 700 Hz
*** we preceded and followed the All-Pass array
*** with Multi-FeedBack Band-Pass OpAmp filters
*** to reduce unwanted side-band signals (away from f(0) = 700 Hz).**

*** Experiments were done using the "UnBalanced" design
*** with (1) AP-Lo at 700 Hz and (12) AP-Hi at 700 Hz
*** to observe the patterns ,with good results.

***** Our design is presented here.
*** (with (1) AP-Lo at 700 Hz and (12) AP-Hi at 700 Hz)

700 Hz All-Pass resonance is based on R=10K and C=23nF.

*** All observations confirm the validity of this design.**

Circuit: #1 Developed working circuit , on next page

***** Using the "UnBalanced" topology**

***** ONE $f(\text{Lo}) = 700 \text{ Hz}$ and Twelve $f(\text{Hi}) = 700 \text{ Hz}$.**

***** 700 Hz resonance is based on $R=10\text{K}$ and $C=23\text{nF}$.**

***** Combined Lo and Hi to produce**

***** a Band-Pass Filter Signal.**

***** U09 and U10 are Voltage Buffers.**

***** U23 "APadjust" is a voltage-combining circuit.**

***** Combining $f(\text{Lo})$ and $f(\text{Hi})$**

***** to produce a Dual-Notched Filter Signal.**

***** Final Filters: Fx02 $Q=5$, and Fx03 $Q=10$**

pull out a very usable Narrow Dual-Notched Band-Pass signal.

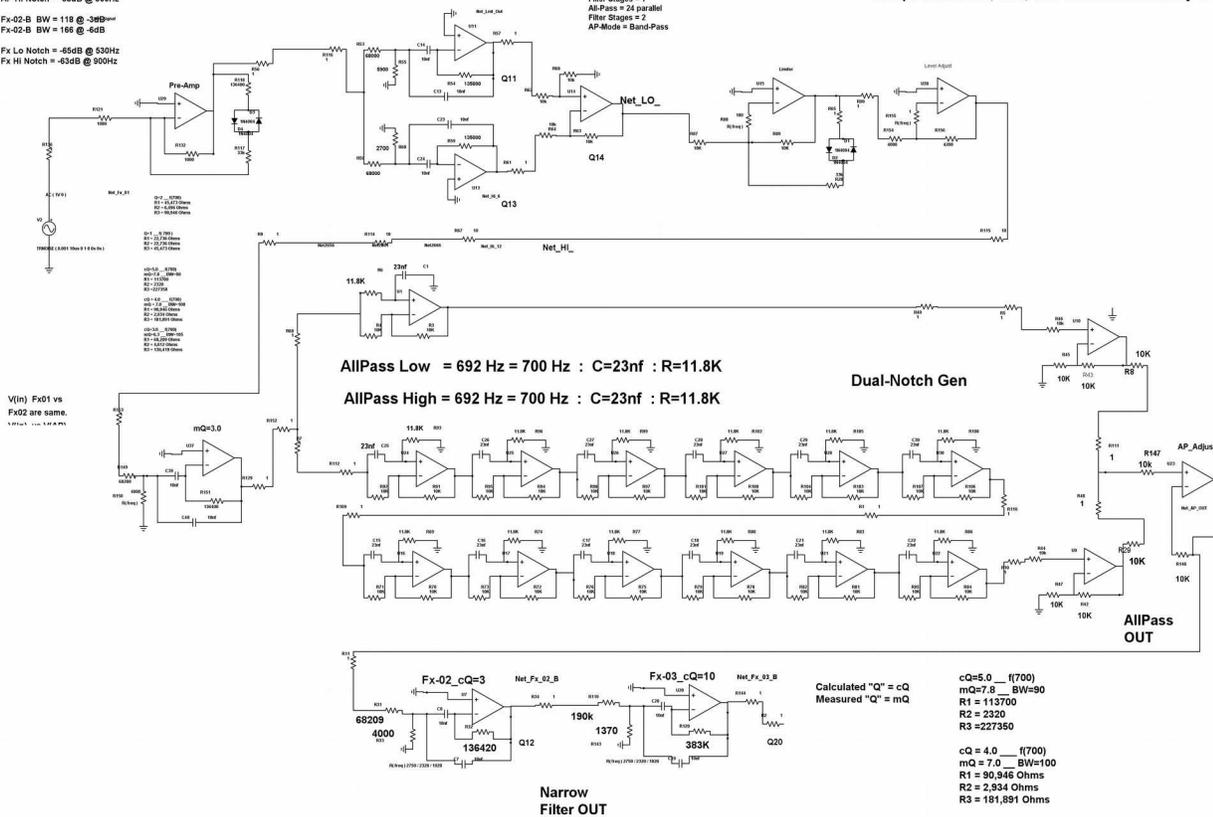
Circuit: "APC" (AP24-1RL-1F-12F-Unb-Sum)

AP24-1RL-1F-12F-Unb-Sum-S-423-21-210827-1536

All-Pass BW = 138 @ -3dB
 All-Pass BW = 192 @ -6dB
 AP Lo Notch = -60dB @ 530Hz
 AP Hi Notch = -60dB @ 900Hz
 Fx-02-B BW = 118 @ -3dB
 Fx-02-B BW = 168 @ -6dB
 Fx Lo Notch = -65dB @ 530Hz
 Fx Hi Notch = -63dB @ 900Hz

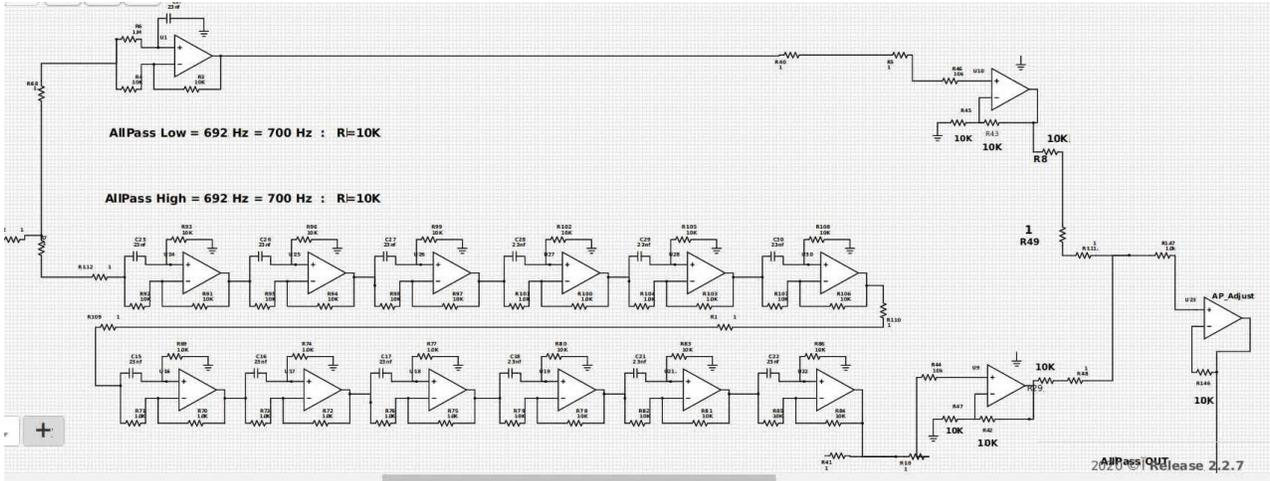
Design Format:
 PreAmp=1
 Roof = 1
 Limiter = 1
 Filter Stages = 1
 All-Pass = 24 parallel
 Filter Stages = 2
 AP-Mode = Band-Pass

ResearchGate.Net,
 Glen Ellis : Univ Tennessee, Memphis, TN ,
 Mark Sitkowski, Ph.D. Design Systems Ltd., Australia,
 Joseph Puncocar, Prof, VSB-Technical University of Ostrava Czech .



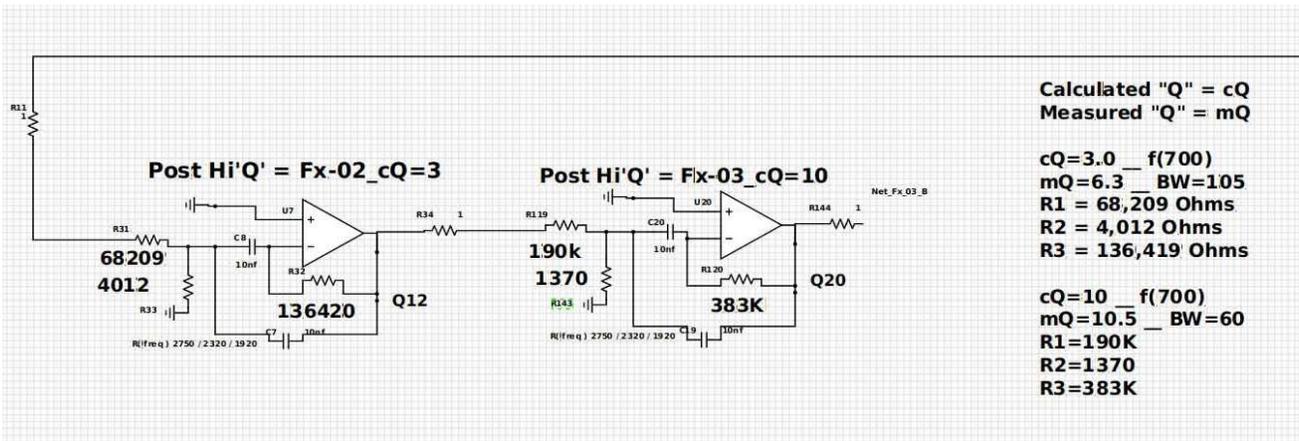
All-Pass Non-Resonant Phase-Filter Band-Pass
which produces Dual-Notch Band-Pass.

Below: Detail: APC
All-Pass module generates Dual-Notches :
The All-Pass-Low and the All-Pass-High are Buffered and Summed
to generate the Narrow Dual-Notch Pass-Band. .



Dual Notch Bode Plot generated from this stage.

Below: Detail: APC
Hi 'Q' Filters sharpen the Band-Pass inside of the Dual-Notches :



Final Filter 03 and Filter 04
are for producing an enhanced Narrow Band-Pass.

Notes: AFC

Bode Plot : **Yellow** trace is AllPass output.
###

Plots LiteBlue, **Red**, DarkBlue show Filter-02 Q=3
when tuned +/- 70 Hz (-3dB)
within the All-Pass Output **Yellow** Trace.

The flat-topped trace is the "Roofing-Filter"
which precedes the Limiter circuit,
Notice the -27 dB per Octave attenuation of side-band signals,
outside of BW=350Hz.

*** This Version used Fx-02 Q=3 (red) and Fx-03 Q=10 (narrow blue)

*** Scale : 700mV = -3dB ; 500mV = -6dB

*** Notch High 900 Hz = -53 dB, Notch BW = 360 Hz

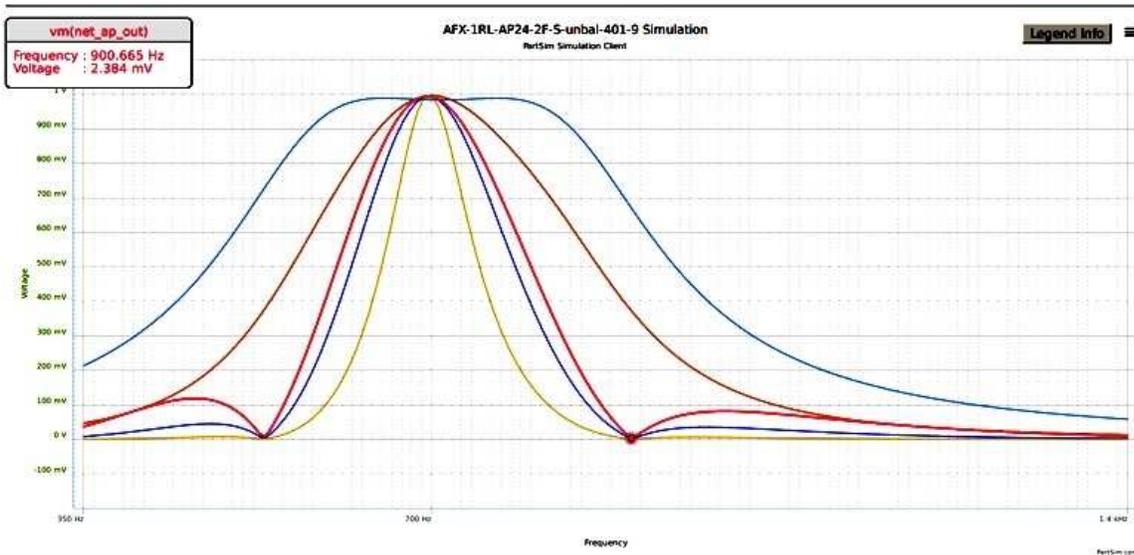
Bode plot : AFC

*** Notice the Dual-Notches **Red** trace, around f(0)

*** **Yellow** trace is the final filter, with Sharp Band-Pass.

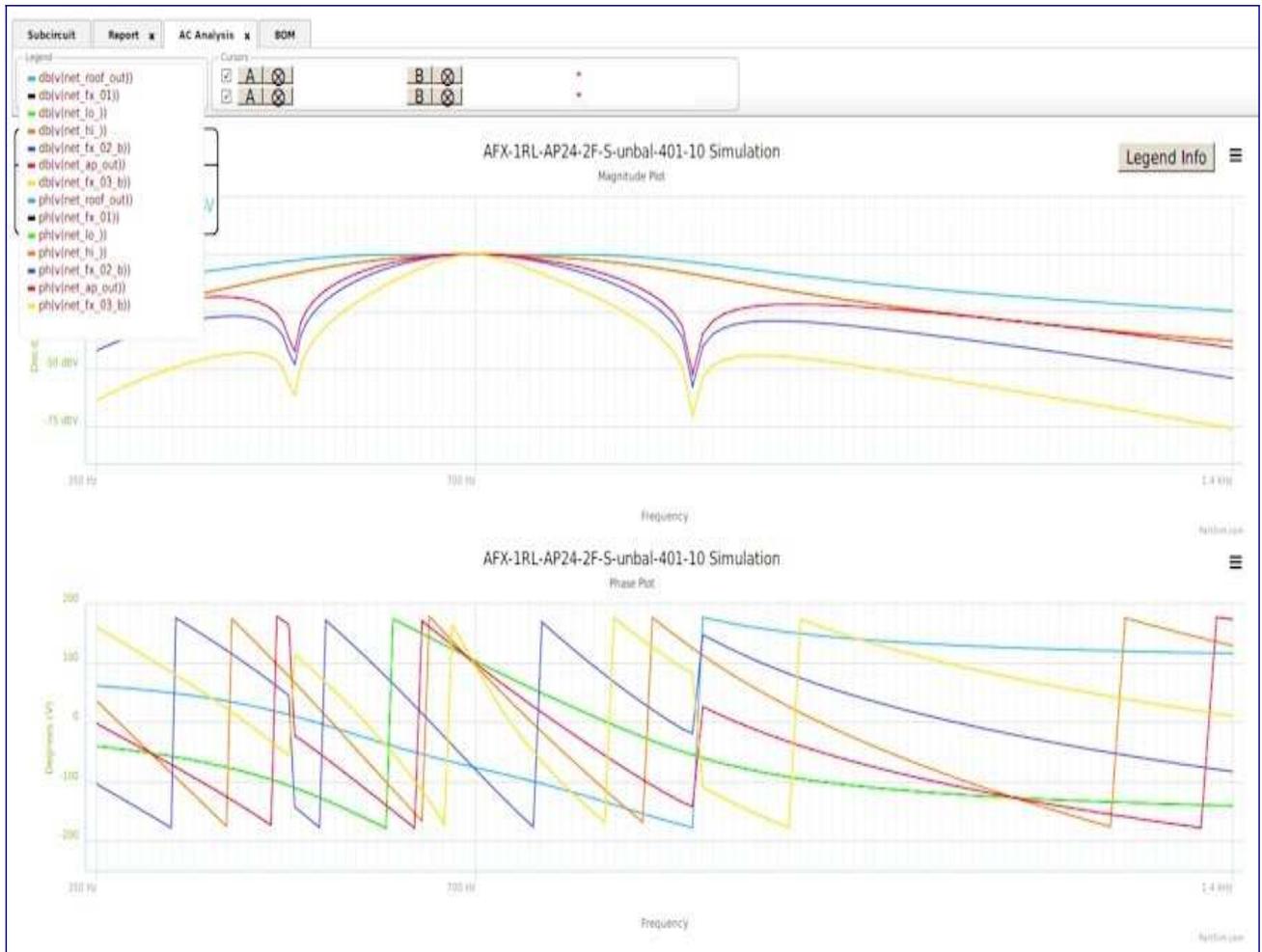
*** Notice: Fx-02 Q=3 and Fx-03 Q=10

are for extremely narrow Band-Pass, inside of Dual-Notches.



Magnitude Plot : AFC

- *** Below : **YELLOW** trace is final Q=20 result shown is the f(0) changed +\| to -3dB points.
- *** f(0) Shifts are confined to the AllPass Output plot.



Magnitude Plot : *** Magnitude Scale readings : V = -dB



*** Magnitude Scale readings : V = -dB
These Band-Pass signals-are NOT a Gaussian Shape.

- *** **Yellow** trace Filter-03 at Hi-Notch = -70 dB
- *** **Yellow** Spreads at the rate of 5.2 Hz per -dB attenuation (approx "**Brick-Wall**").

Circuit: **AFX_3RL-F8AFQ**

Special Advanced All-Pass Band-Pass circuit combining AFX and APC concepts.

***** Two Variable MFB Filters**

with 8 All-Pass stages inserted in the middle

An effective combo-design, which is simpler

but not as effective as the AFX'V'-3RL-V4F-D-VQ version.

Result One Dual-Pot can control $f(0) \pm 75$ Hz, reading at the -3dB level.

AFX-F8AFQ-S-411T-4-210818-0700

Notch Hi Depth -55 dB and -83 dB
Notch Lo Depth -38 dB and -70 dB
Differential Notches at 920 & 920

Purpose:

Design of a notch filter with a notch depth of -55 dB and -83 dB, and a notch width of 10 Hz. The notch is centered at 920 Hz. The filter is designed using two MFB filters and eight all-pass stages.

*** Diff-Dual-Notch Results ***

Notch Hi Depth: -55 dB

Notch Lo Depth: -38 dB

Differential Notches: 920 Hz

Notch Width: 10 Hz

Center Frequency: 920 Hz

Quality Factor: 10

Gain: 0 dB

Phase: 0 degrees

Roll-off: 20 dB/decade

Stopband Attenuation: -55 dB

Passband Ripple: 0.1 dB

Group Delay: 0 ns

Phase Delay: 0 degrees

Phase Shift: 0 degrees

Phase Slope: 0 degrees/decade

Phase Intercept: 0 degrees

Phase Offset: 0 degrees

Phase Error: 0 degrees

Phase Tolerance: 0 degrees

Phase Resolution: 0 degrees

Phase Accuracy: 0 degrees

Phase Precision: 0 degrees

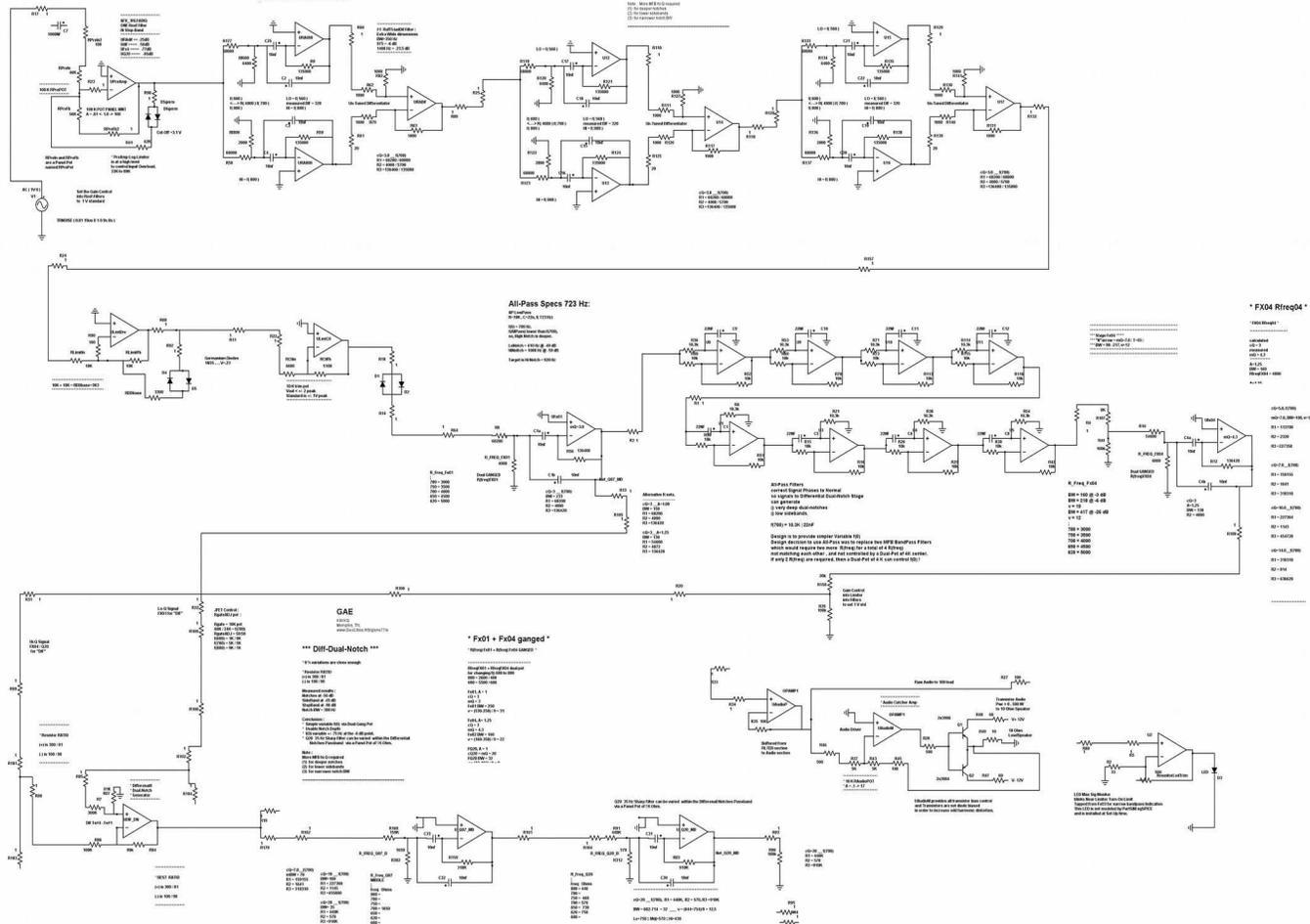
Phase Stability: 0 degrees

Phase Consistency: 0 degrees

Phase Reliability: 0 degrees

Phase Robustness: 0 degrees

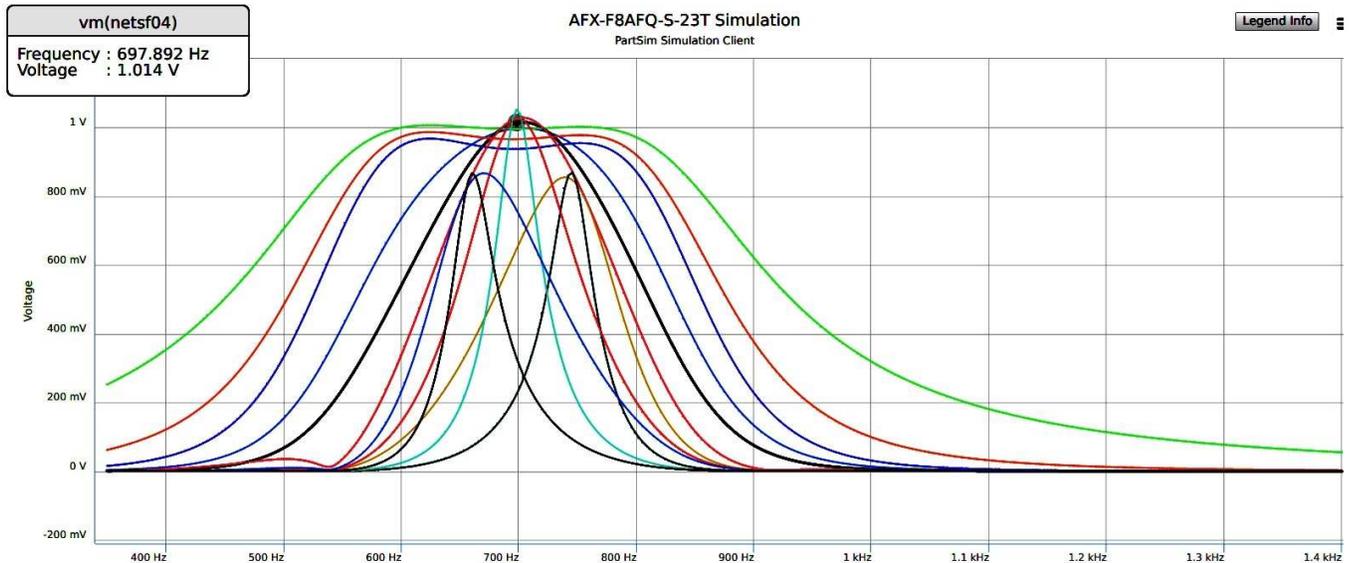
Phase Resilience: 0 degrees



* FX04 Rfreq04 *

Component	Value
R1	10k
R2	10k
R3	10k
R4	10k
R5	10k
R6	10k
R7	10k
R8	10k
R9	10k
R10	10k
R11	10k
R12	10k
R13	10k
R14	10k
R15	10k
R16	10k
R17	10k
R18	10k
R19	10k
R20	10k
R21	10k
R22	10k
R23	10k
R24	10k
R25	10k
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R82	10k
R83	10k
R84	10k
R85	10k
R86	10k
R87	10k
R88	10k
R89	10k
R90	10k
R91	10k
R92	10k
R93	10k
R94	10k
R95	10k
R96	10k
R97	10k
R98	10k
R99	10k
R100	10k

Bode Plot : **AFX_3RL-F8AFQ**



Results: **AFX_3RL-F8AFQ with Dual-Notches.**

*** Compared to the AFX'V' ("AFV-3RL-V4F-D-VQ" version)

(1) BW @ -3dB is wider ;
160 Hz vs 90 Hz.

(2) Dual Notch BW is wider ; 380 Hz vs 330 Hz.
but the FX Q20 will narrow this to 35Hz.

(3) Variability of $f(0)$ is much narrower ; +/- 75 Hz is good (at -3dB),
vs +/- 100 Hz for the AFX'V' versions.

At $f(700 \text{ Hz})$, +/- 75 Hz is similar to +/- one piano note.

Changing the $f(0)$ of the All-Pass stages and/or the gain of AP stages

(1) will change the $f(0)$ of the AP notches up/dn factor of 2.

(2) will change the Band-Width of the notches w/n factor of 2..

$F(700)$ is best freq for the intended usage of this Filter Circuit ,
and is a compromise the author selected for this project.

(4) Variable $f(0)$ controlled physically
by a Single Panel-Mounted dual-gang Pot
is a good feature, even if not very much variation.

Magnitude Plot: **AFX_3RL-F8AFQ**

Magnitude Plot clearly shows the Notch Depth while shifting $f(0) \pm 100$ Hz

*** Notch Generator freq tracks with $f(0)$

*** at ± 100 Hz

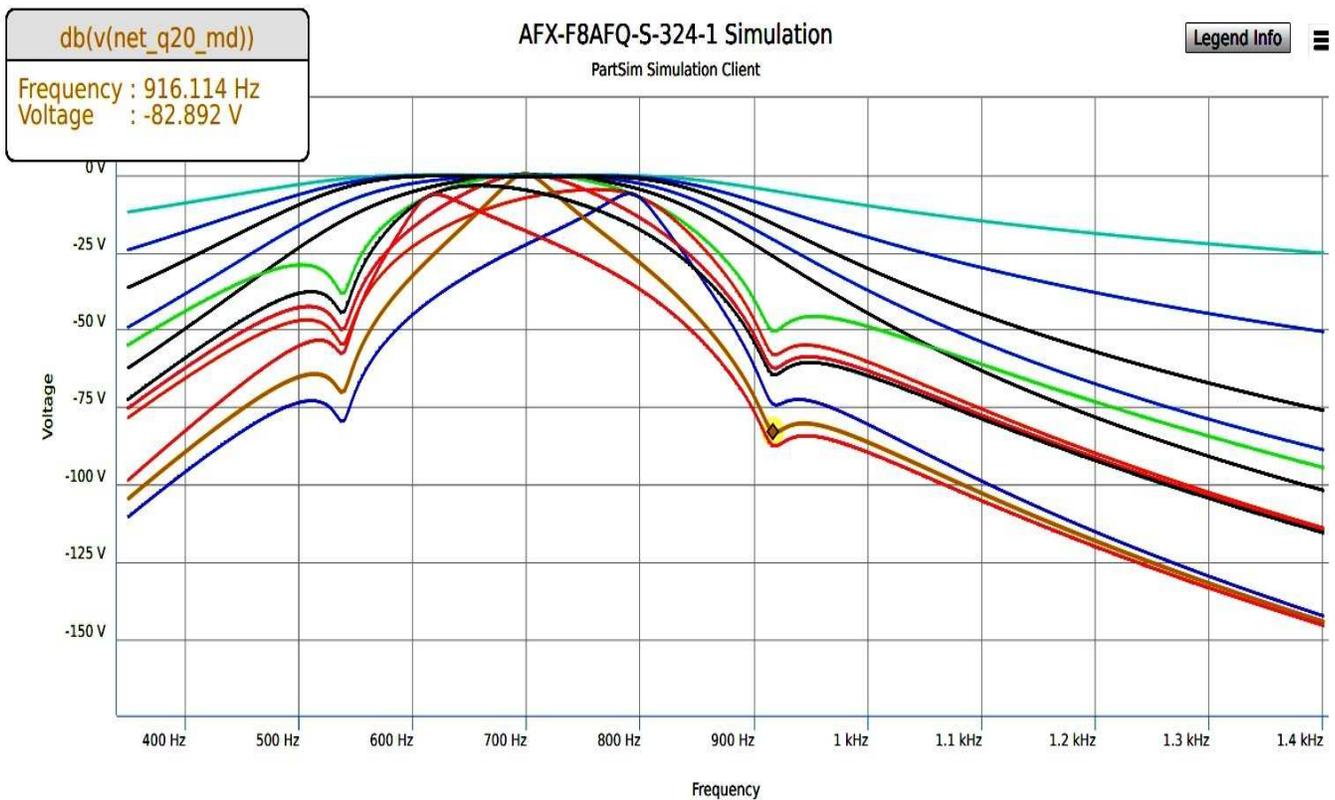
*** $F_x(100\text{Hz})$ is -0.5dB down

*** $F_x(35\text{Hz})$ is -1.0dB down

*** At $f(700)$ normal settings

Deep Notch (Yellow/Black trace)

is -82 dB 920Hz .



note:

*** Also authors explored the "UnBalanced" (7 Hz and 700 Hz) approach.

*** The All-Pass-Lo is tuned to 6.20 Hz (aprox. 7 Hz)

*** The All-Pass-Hi is tuned to 692 Hz. (aprox. 700 Hz)

*** Results: equal success in circuit performance.

*** Further experiments were done using the "UnBalanced" design

*** with $f(0)$ at 70, 137, 175, 350, 650 Hz vs. 750 Hz

to observe the patterns, with good results.

*** Further experiments were done using the "UnBalanced" design

*** with filter pairs of 2, 4, 6, 8, 10, 12, 14, 16, 18, 24

to observe the patterns ,with good results.

*** These circuits are not discussed in this paper.

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