

Chapter: **AFX 'V'ariable**



this is the Best-of-AFX Phase-Filter Circuit Design

Non-Resonant Dual-Notch Phase-Filter-

******* Goals achieved in AFX-'V' :**

- *** (1) Simpler design,**
- *** (2) Simpler construction,**
- *** (3) Simpler adjustment.**
- *** (4) Enhanced Variability $f(0)$**

Continued Design features from AFX:

***** Improved design from building-block modules**

**3 Filters are $Q=3$, 1 Filter $Q=5$,
all $R(\text{freq})$ aprox. Same.**

Enables use of single control of four $R(\text{freq})$ stages.

***** Designed so that the High 'Q' Sharp Filter is also variable
within the main band-pass.**

***** Designed so that the Dual-Notches
are < -60 dB and the Stop-Band < -100 dB .**

Design choices:

*** Simple repetitive application of Modified *Delyannis-Friend*-Multiple-FeedBack design.

*** MFB topology was chosen because :

- *** (1) input vs output impedances match well, loading is naturally controlled.
- *** (2) single resistor frequency control each stage.
- *** (3) frequency adjustments alters gain by only the square-root of the f(change) .

Just for reference:

Delyannis-Friend Multiple-Feed-Back design

MULTIPLE FEEDBACK BAND-PASS DESIGN EQUATIONS

$$\frac{-H \omega_0 s}{s^2 + \alpha \omega_0 s + \omega_0^2}$$

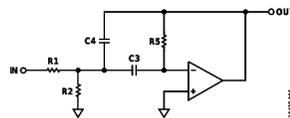


Figure 6.

$$\frac{V_o}{V_{in}} = \frac{-s \frac{1}{R_1 C_4}}{s^2 + s \frac{C_3 + C_4}{C_3 C_4 R_5} + \frac{1}{R_5 C_3 C_4} \left(\frac{1}{R_1} + \frac{1}{R_2} \right)}$$

To design the filter, choose C3.

Then

$$k = 2 \pi F_0 C_3$$

$$C_4 = C_3$$

$$R_1 = \frac{1}{H k}$$

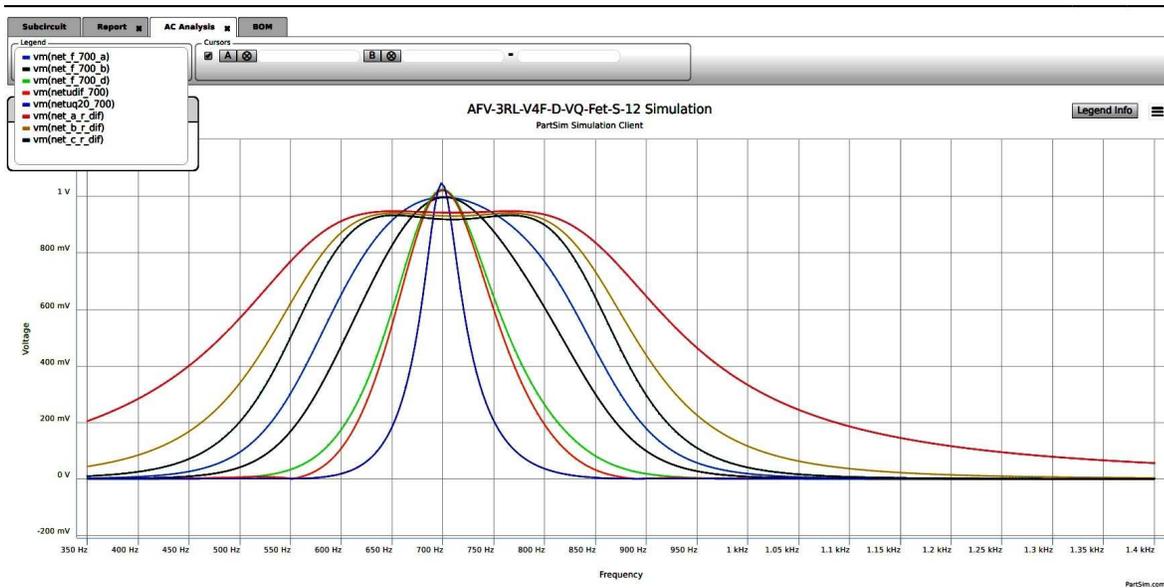
$$R_2 = \frac{1}{(2Q - H)k}$$

$$R_5 = \frac{2Q}{k}$$

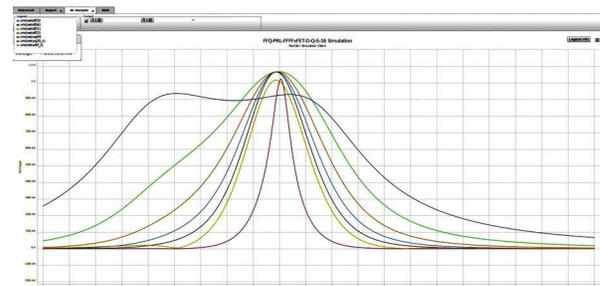
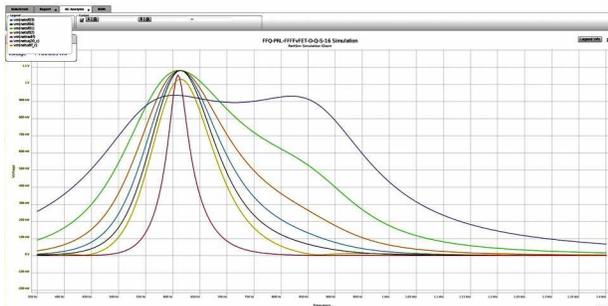
Delyannis-Friend Multiple-Feed-Back design

Bode Plot: **AFV-3RL-v4F-D-vQ-Fet**

Roofing Filter Output is (red), very wide which contains the variability of the central f() signal



****** Below : shown adjusted 600Hz , 700Hz , 800Hz**
******* Notice that the peak amplitudes of the final signals stay within 0.3 dB of the f(700) signal.**



f() signal

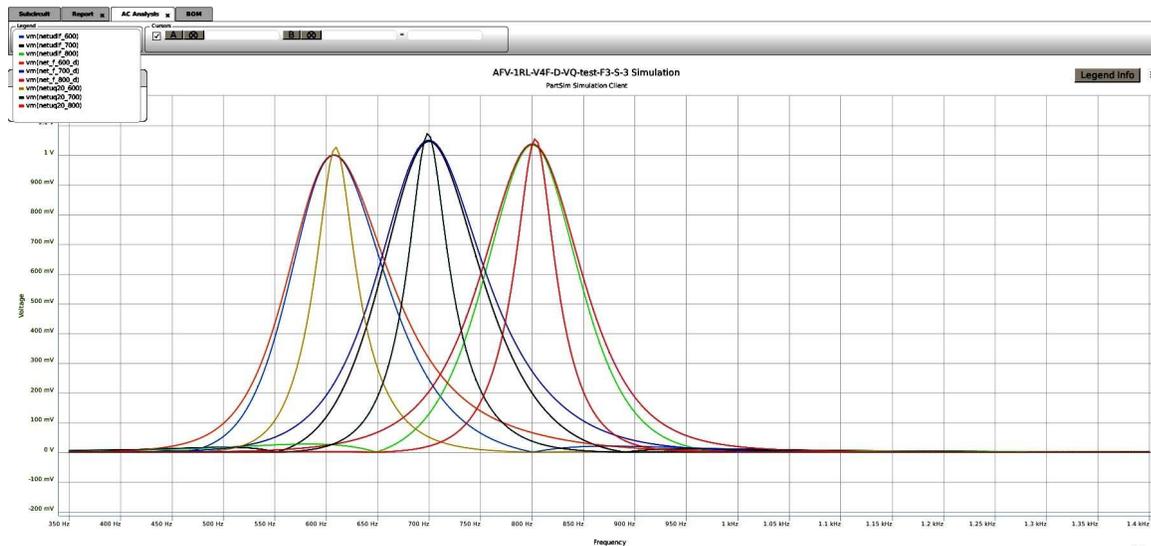
variability of the central

Notice that the 600 --- 800 waveforms have good central Band-Pass shapes.

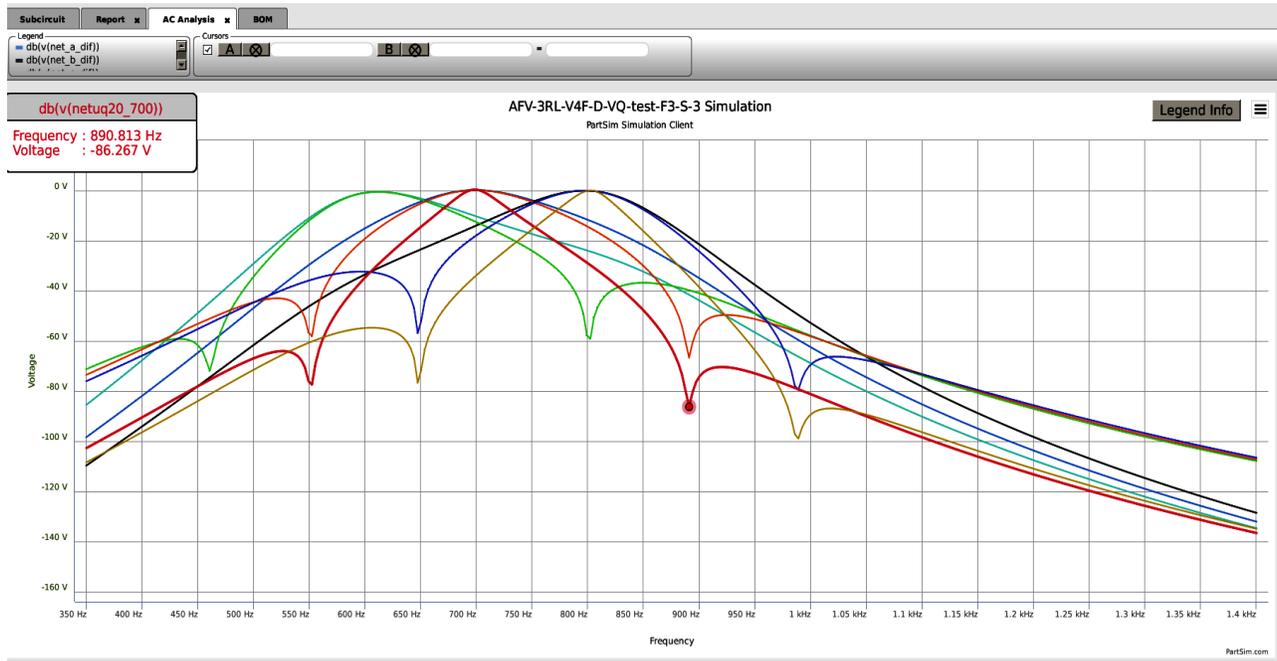
Bode Plot: **advanced AFV circuit** utilizes
Three Triad-Roofing-Differential Filters for for max sideband control.

- *** **Dual-Notches** are very Deep and Octave Stop-Band very low.
- *** **Main Filter f(0)** is Variable 600 - 700 - 800 by user in real-time.
- *** **Sharp Q=20** filter is variable within the selected PassBand.

- *** Here, the R(freq) is currently controlled by one R(freq) Pot, which can be mounted on the front panel, for real-time control.
- *** The Four FET controllers are driven by a single Voltage Source, controlled by a Panel Mounted Pot.
- *** Front Panel Rotary Switch allows User to send any stage into the Audio Section.
- *** Front Panel Switch can be utilized to drive FxQ20 from any filter stage.



Magnitude Plot: **AFV-3RL-v4F-D-vQ-Fet**



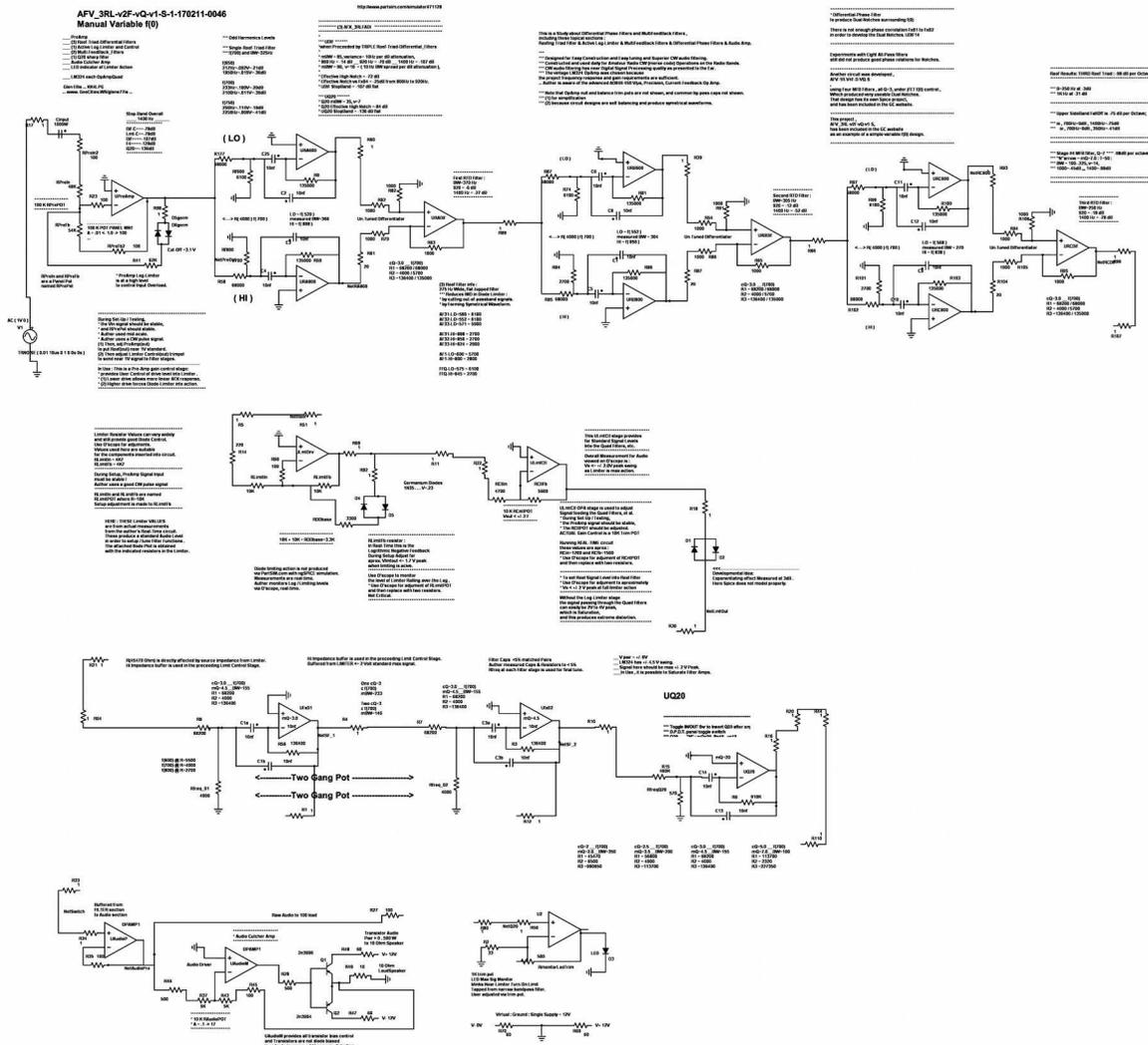
*** At 900 Hz, the **Red Dot on Notch** indicates **-86 dB attenuation** for the **f(700)** trace . Trace to 1400 Hz is -76 dB attenuation.

circuit: **Sample: 'AFV_3RL-v2F-vQ-v1-S'**

This simple circuit was NOT spectacular but was given a fair test.

... Goal was to prove the use of only **Two MFB filters** which would require only a single dual-Pot for control of $f(0)$..

- *** AFV_3RL-v2F-vQ-v1-S design :
- *** (1) with **Three Roof Filters**
- *** (2) with only **Two MFB filter stages**
- *** (3) with R(freq) controlled by a **Two-Gang Pot**



Results: use of only **Two MFB filters**

which would require only a single dual-Pot for control of $f(0)$..

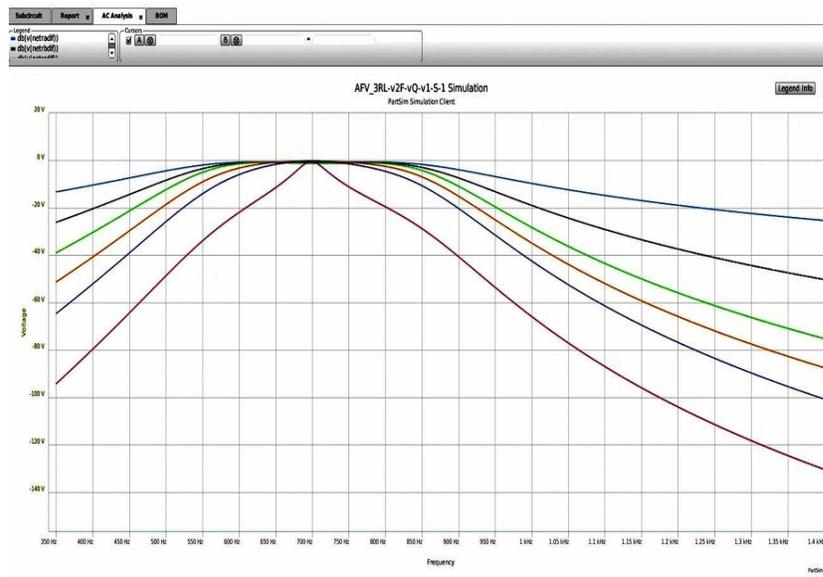
... **Dual Notches could not be well developed when using only Two MFB filters.**

... **More Phase-Alignment in the filter module is required to generate the Dual Notches.**

... **Therefore,**

No notches are presented in the below plots, and this is the best Bode Plot .

The Sharp Band-Pass comes from the two $Q=3$ final filters.







Chapter: **AFX_Filter_“T”**

Non-Resonant Dual-Notch Phase-Filter-

An AFX filter

Emphasizing the Roofing Filters “T” to supress the sidebands

- *** Triple Roof-Triad-Differential Filters preparing the signals**
- *** to drive a single Q=7 MFB bandpass filter**
- *** Triple Roof-Triad-Filter is 1400 Hz = -76 dB per octave.**
- *** Last stage Q=7 MFB is 1400 Hz = -98 dB per octave.**
- *** Last stage Q=20 MFB is 1400 Hz = -110 dB per octave.**

***** Roof-Triad-Filter info :**

***** all sections with same f(0) and same components .**

***** design is very tolerant of minor component variations .**

***** “cQ” is the calculated ‘Q’ for each stage :**

f(585) cQ=3.0 R(5800)

f(700) cQ=3.0 R(4000)

f(830) cQ=3.0 R(2800)

***** “mQ” is the measured ‘Q’ accumulated through to the last stage.**

Results: **AFT_v1-3-S-p1**

Roof Results: FIRST Roof Triad

calc design BW=325 Hz at -3dB
*** ie , 700Hz=0dB , 1400Hz=-26dB
*** ie , 700Hz=0dB , 350Hz=-13dB
*** SideBand Falloff is -26 dB per Octave;

Roof Results: SECOND Roof Triad

calc design BW=325 Hz at -3dB
*** ie , 700Hz=0dB , 1400Hz=-54dB
*** ie , 700Hz=0dB , 350Hz=-15dB
*** SideBand Falloff is -54 dB per Octave;

Roof Results: THIRD Roof Triad

calc design BW=325 Hz at -3dB
*** ie , 700Hz=0dB , 1400Hz=-75dB
*** ie , 700Hz=0dB , 350Hz=-18dB
*** SideBand Falloff is -75 dB per Octave;

*** Design for Sharp Filter *****

calc Design Final MFB filter, Q=7
*** BW = 100 @ -3 dB range=100---225, v=14,
*** 1000 Hz=-45dB ,, 1400 Hz = -98 dB

*** Cumulative Results after the Sharp Filter

*** cumulative measured results : Q=20
*** cumulative measured -98dB per octave
*** BW = 35 @ -3dB , range 35---126, v= 10,
*** 1000 Hz=-75dB ,, 1400 Hz = -110 dB

Chaper : AFX_pFilter_2_AFT ..210807... 4/7

Bode Plot: **AFT_v1-3-S-p1**

Triple Roof-Triad-Differential Filters plus one Q7 Filter. .

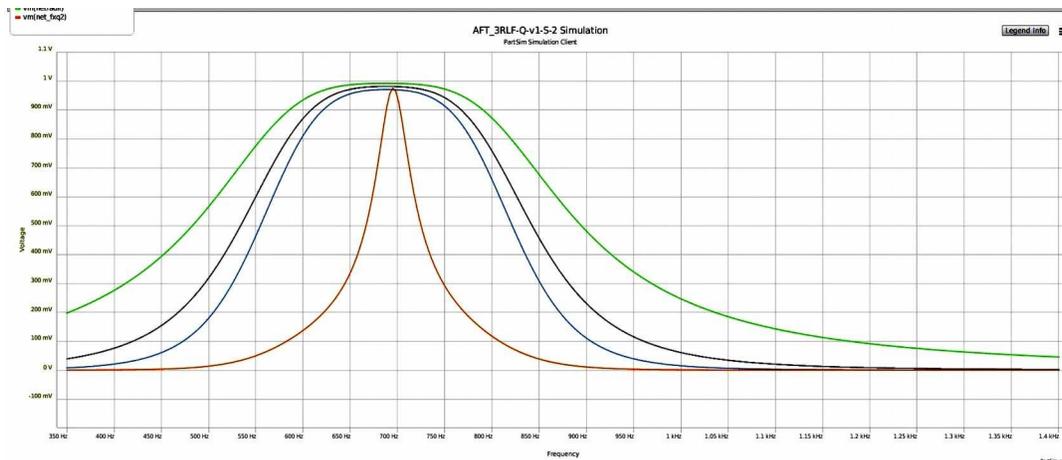
Most complex waveforms displayed.

Red trace is Q=7 signal **Before** Roofing Filters.

Yellow trace is Q=7 signal **After** Roofing Filters.



***** Notice the Roof Filters contribute to sideband suppression.**

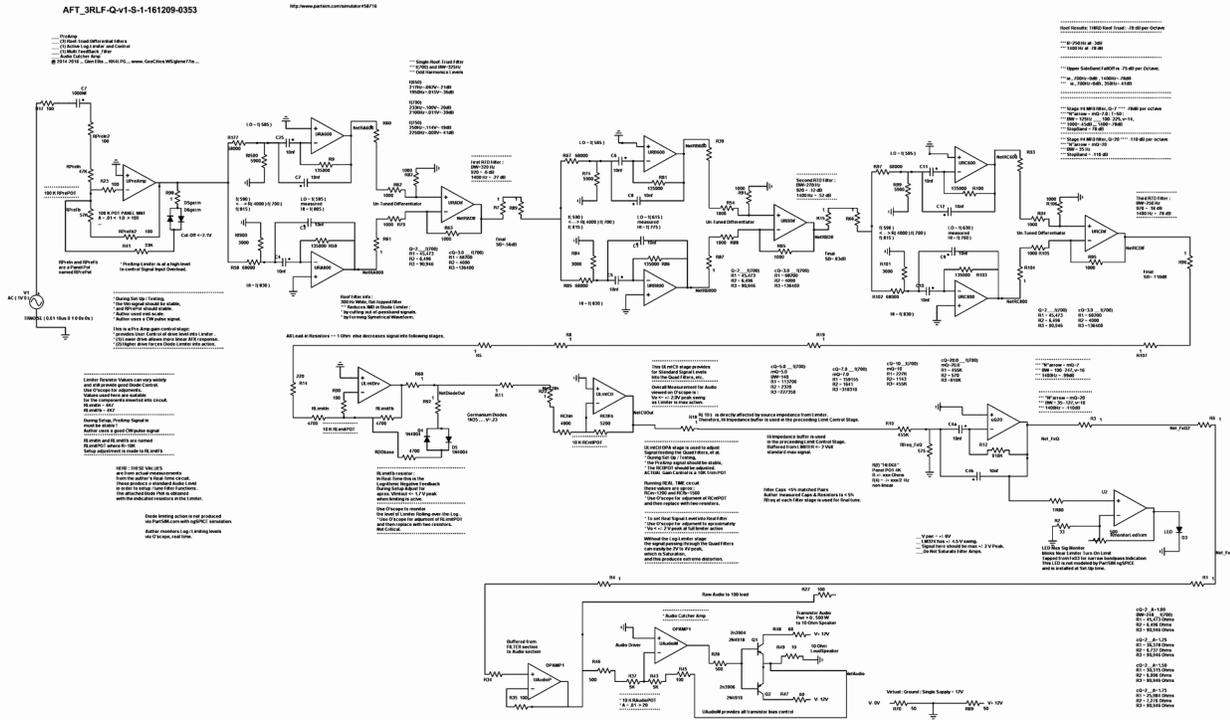


Circuit: **AFT_v1-3-S-p1**

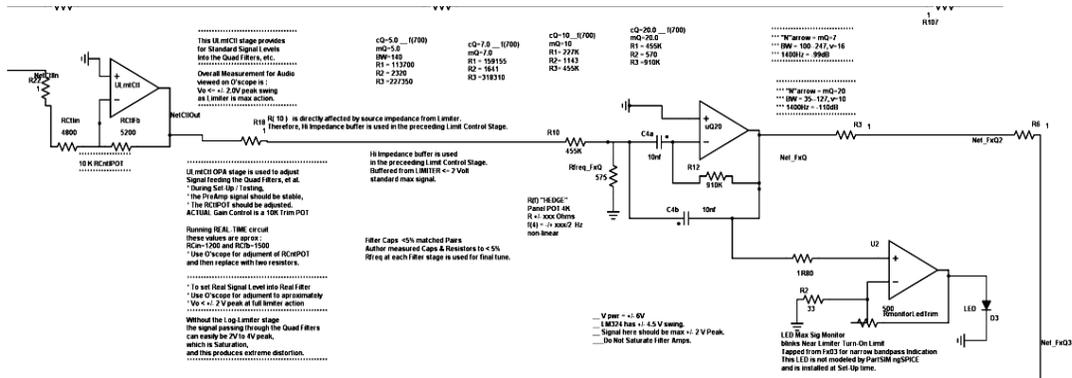
a Developed 'AFT' Circuit

*** No Dual Notches ***

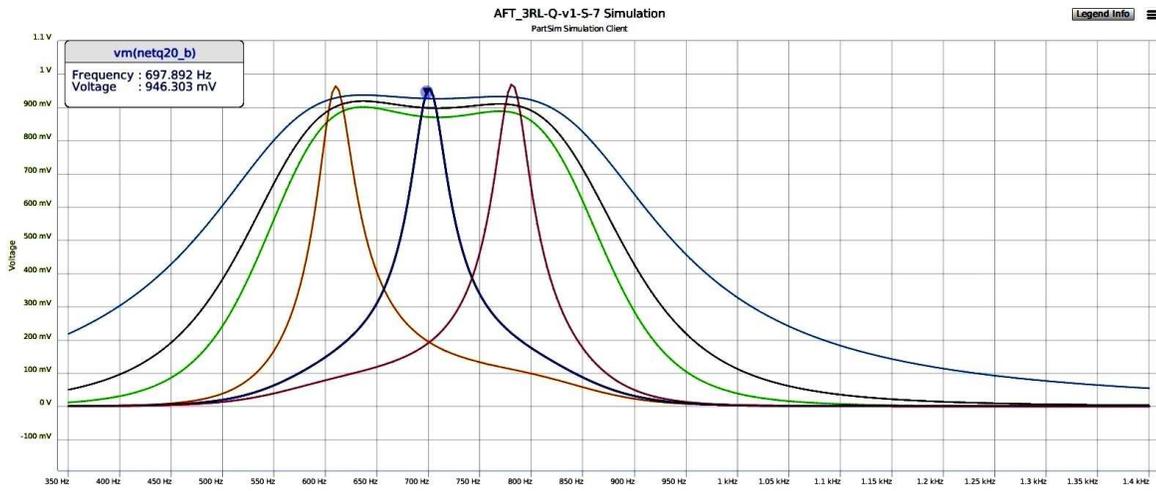
with PreAmp + three Roof-Filters + Active-Limiter + Q20 Filter + Audio :



Circuit: for single Narrow Filter:



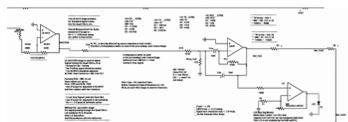
Bode Plot : **AFT_v1-3-S-p1**



f(0) adjusted 600 - 700-- 800

Chaper : AFX_pFilter_2_AFT ..210807... 7/7





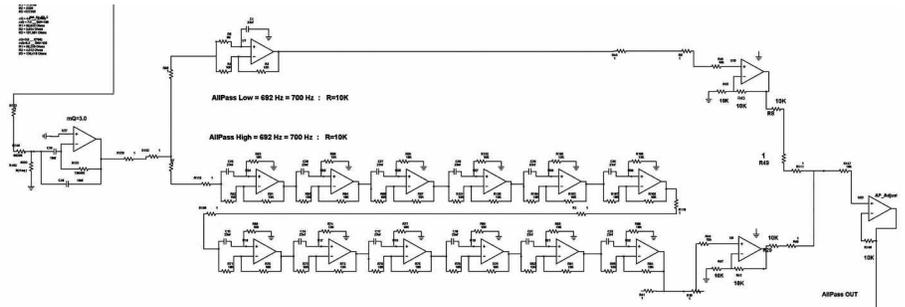
Chapter: All-Pass Band-Pass Filter



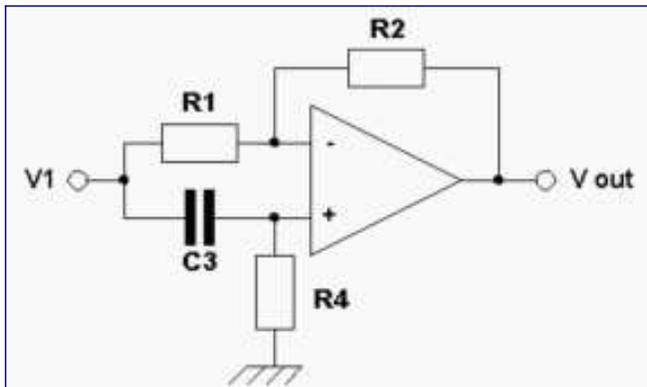
Phase-Filter Non-Resonant Dual-Notch

We examine a Phase-Filter-built from All-Pass Filters

Circuit: AFC core
1Lo-12Hi All-Pass

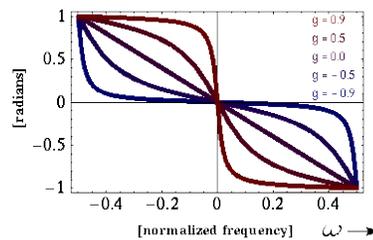


Some Electrical Theory
from common Electrical Engineering textbooks :



First-Order Allpass Phase Response (let $g = r e^{j\theta}$)

$$\Theta(\omega) \triangleq \angle H(e^{j\omega}) = -\omega - 2 \tan^{-1} \left[\frac{r \sin(\omega - \theta)}{1 - r \cos(\omega - \theta)} \right]$$



"The All-Pass filter has **frequency responses** which **must be zero at $w=0$ and at $w=\pi$.**" [wiki](#)

This paper presents

a Non-Resonant Dual-Notch Phase-Filter

producing a Band-Pass function

as an “ngSPICE project”

produced via the PartSIM.com browser based Simulator.

Introduction:

In all researched texts, the traditional academic texts specify

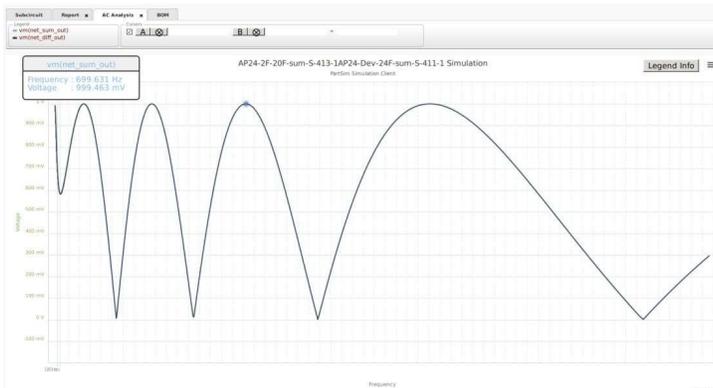
that **All-Pass** filters **Can NOT** be used

for **Low-Pass** nor **High-Pass** functions ,

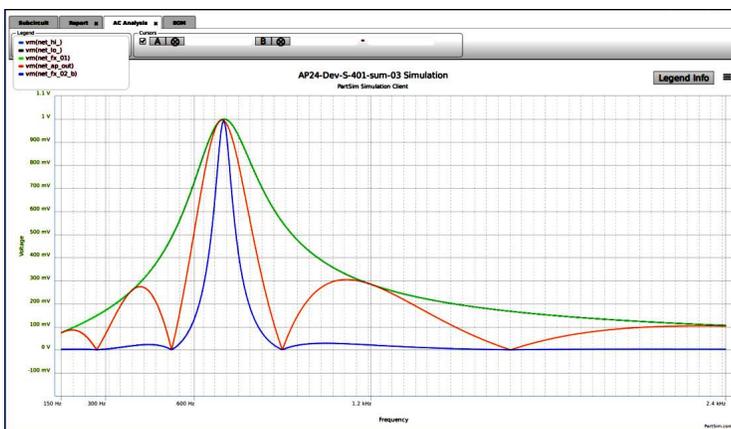
nor for **Band-Pass** functions.

*** However, the author has developed
working **Dual-Notch Band-Pass** circuits

*** which utilize the **All-Pass Filter**
in both LoPass and HiPass configurations



*** Raw All-Pass



*** Bode Plot
of “APC” circuit
All Vout signals

In this #1 circuit,
f(Lo) = 700 Hz and f(Hi) = 700 Hz
This accentuated the "w" notches at :
each "0" point
each "pi" point
in the spectrum.

***** In the #1 fully developed working circuit,**
***** based on normal f(Lo) = 700 Hz and f(Hi) = 700 Hz**
***** we preceded and followed the All-Pass array**
***** with Multi-FeedBack Band-Pass OpAmp filters**
***** to reduce unwanted side-band signals (away from f(0) = 700 Hz).**

***** Experiments were done using the "UnBalanced" design**
***** with (1) AP-Lo at 700 Hz and (12) AP-Hi at 700 Hz**
***** to observe the patterns ,with good results.**

***** Our design is presented here.**
***** (with (1) AP-Lo at 700 Hz and (12) AP-Hi at 700 Hz)**

700 Hz All-Pass resonance is based on R=10K and C=23nF.

*** All observations confirm the validity of this design.**

Circuit: #1 Developed working circuit , on next page

***** Using the "UnBalanced" topology**

***** ONE $f(\text{Lo}) = 700 \text{ Hz}$ and Twelve $f(\text{Hi}) = 700 \text{ Hz}$.**

***** 700 Hz resonance is based on $R=10\text{K}$ and $C=23\text{nF}$.**

***** Combined Lo and Hi to produce**

***** a Band-Pass Filter Signal.**

***** U09 and U10 are Voltage Buffers.**

***** U23 "APadjust" is a voltage-combining circuit.**

***** Combining $f(\text{Lo})$ and $f(\text{Hi})$**

***** to produce a Dual-Notched Filter Signal.**

***** Final Filters: Fx02 $Q=5$, and Fx03 $Q=10$**

pull out a very usable Narrow Dual-Notched Band-Pass signal.

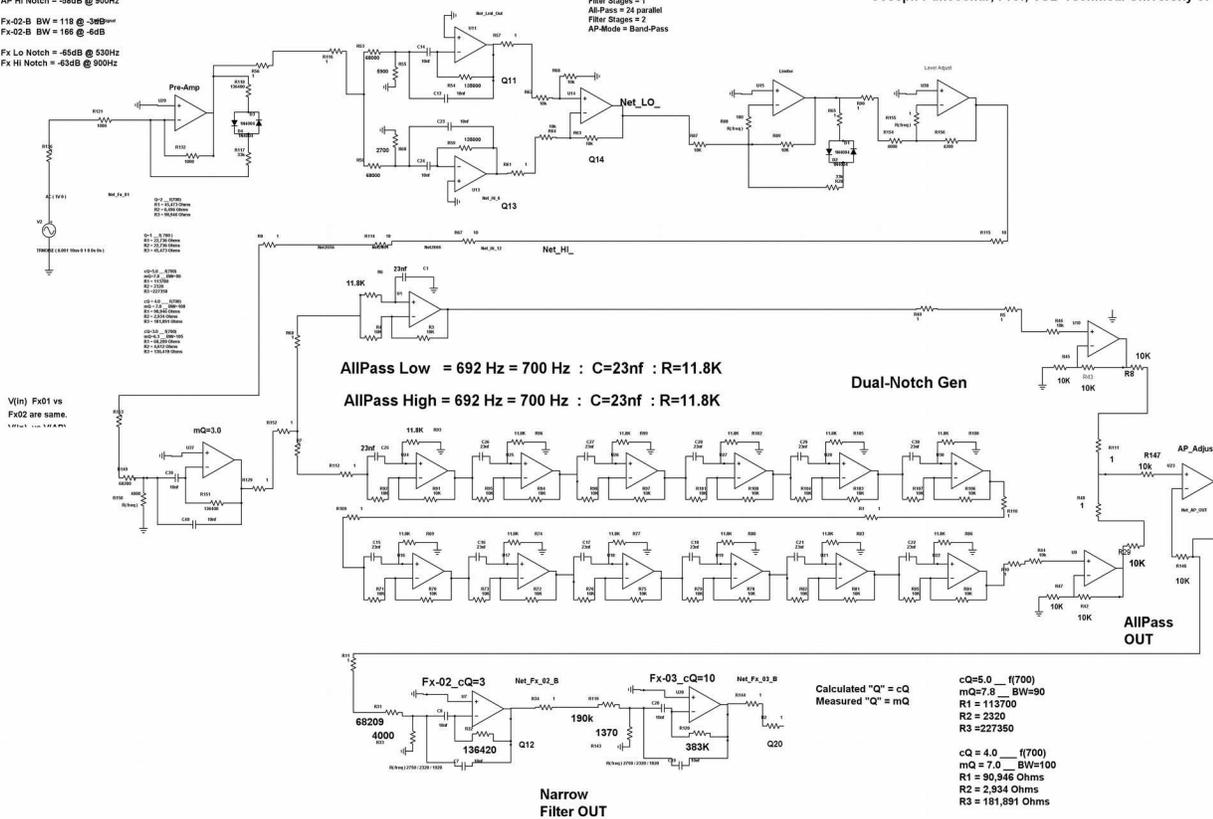
Circuit: "APC" (AP24-1RL-1F-12F-Unb-Sum)

AP24-1RL-1F-12F-Unb-Sum-S-423-21-210827-1536

All-Pass BW = 138 @ -3dB
 All-Pass BW = 192 @ -6dB
 AP Lo Notch = -60dB @ 530Hz
 AP Hi Notch = -60dB @ 900Hz
 Fx-02-B BW = 118 @ -3dB
 Fx-02-B BW = 168 @ -6dB
 Fx Lo Notch = -65dB @ 530Hz
 Fx Hi Notch = -63dB @ 900Hz

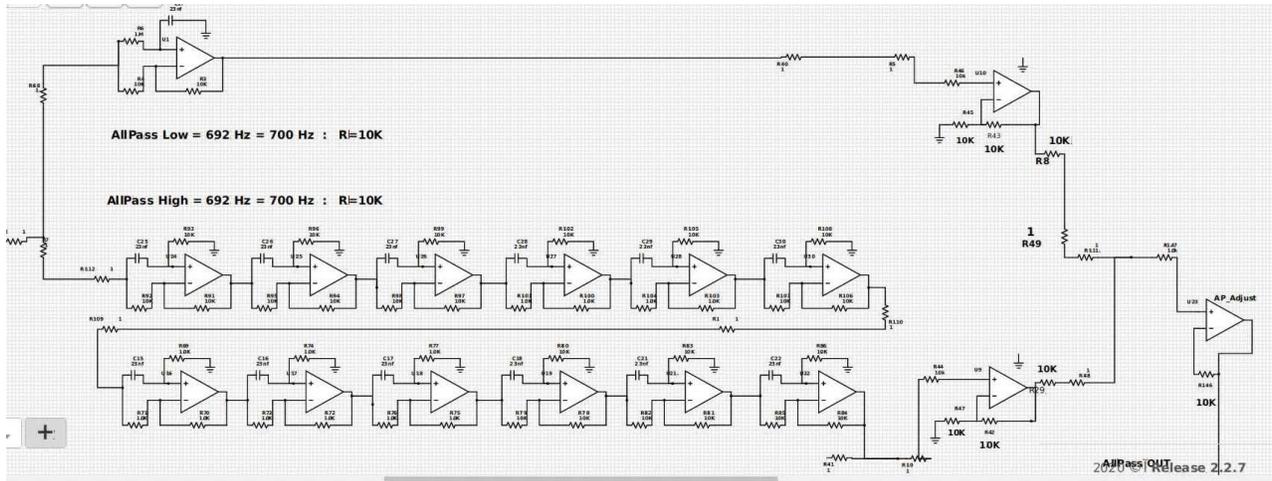
Design Format:
 PreAmp=1
 Roof = 1
 Limiter = 1
 Filter Stages = 1
 All-Pass = 24 parallel
 Filter Stages = 2
 AP-Mode = Band-Pass

ResearchGate.Net,
 Glen Ellis : Univ Tennessee, Memphis, TN ,
 Mark Sitkowski, Ph.D. Design Systems Ltd., Australia,
 Joseph Puncochar, Prof, VSB-Technical University of Ostrava Czech .



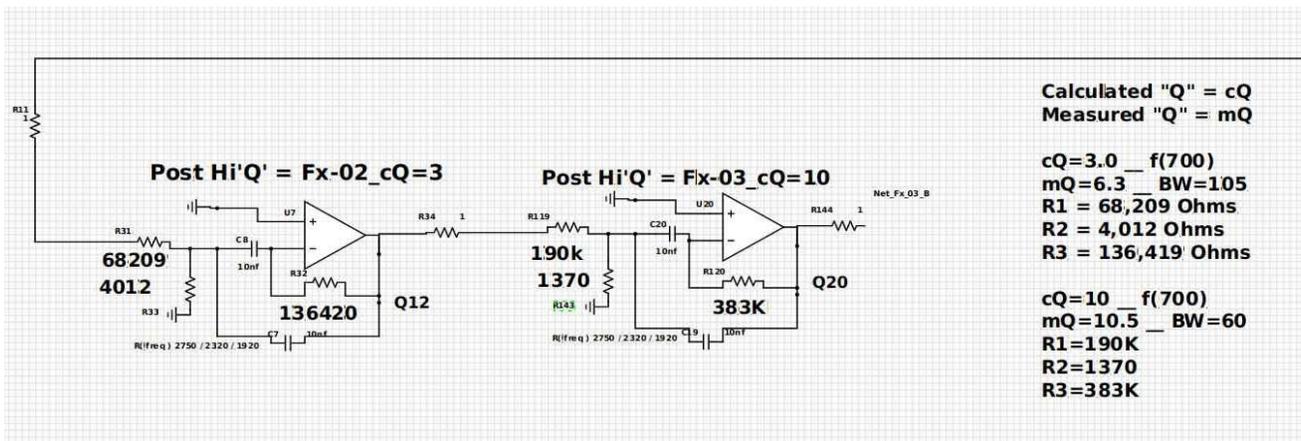
All-Pass Non-Resonant Phase-Filter Band-Pass
 which produces **Dual-Notch Band-Pass**.

Below: Detail: APC
All-Pass module generates Dual-Notches :
The All-Pass-Low and the All-Pass-High are Buffered and Summed
to generate the Narrow Dual-Notch Pass-Band. .



Dual Notch Bode Plot generated from this stage.

Below: Detail: APC
Hi 'Q' Filters sharpen the Band-Pass inside of the Dual-Notches :



Final Filter 03 and Filter 04
are for producing an enhanced Narrow Band-Pass.

Notes: AFC

Bode Plot : **Yellow** trace is AllPass output.
###

Plots LiteBlue, **Red**, DarkBlue show Filter-02 Q=3
when tuned +/- 70 Hz (-3dB)
within the All-Pass Output **Yellow** Trace.

The flat-topped trace is the "Roofing-Filter"
which precedes the Limiter circuit,
Notice the -27 dB per Octave attenuation of side-band signals,
outside of BW=350Hz.

*** This Version used Fx-02 Q=3 (red) and Fx-03 Q=10 (narrow blue)

*** Scale : 700mV = -3dB ; 500mV = -6dB

*** Notch High 900 Hz = -53 dB, Notch BW = 360 Hz

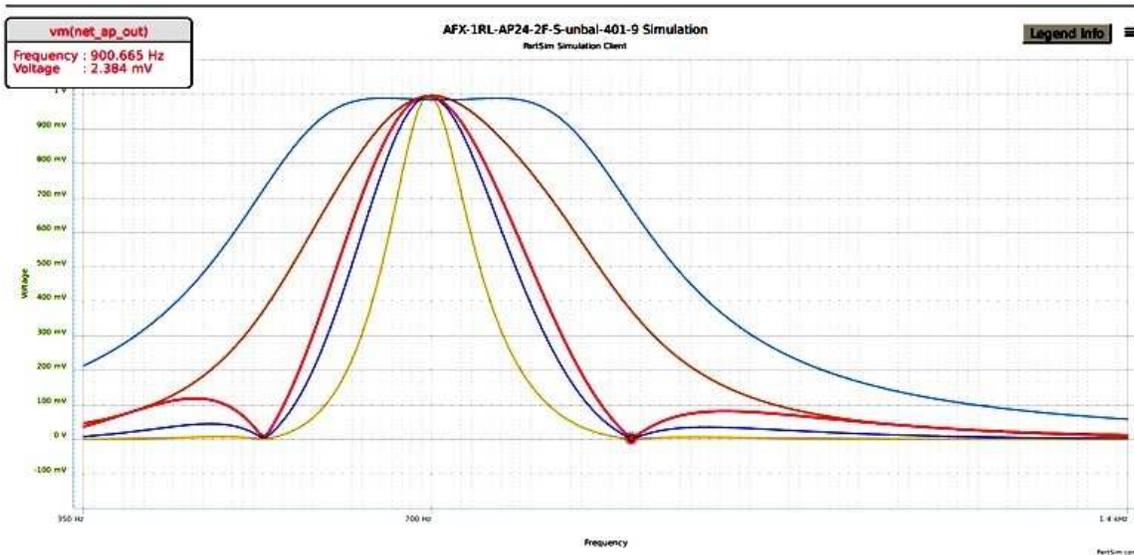
Bode plot : AFC

*** Notice the Dual-Notches **Red** trace, around f(0)

*** **Yellow** trace is the final filter, with Sharp Band-Pass.

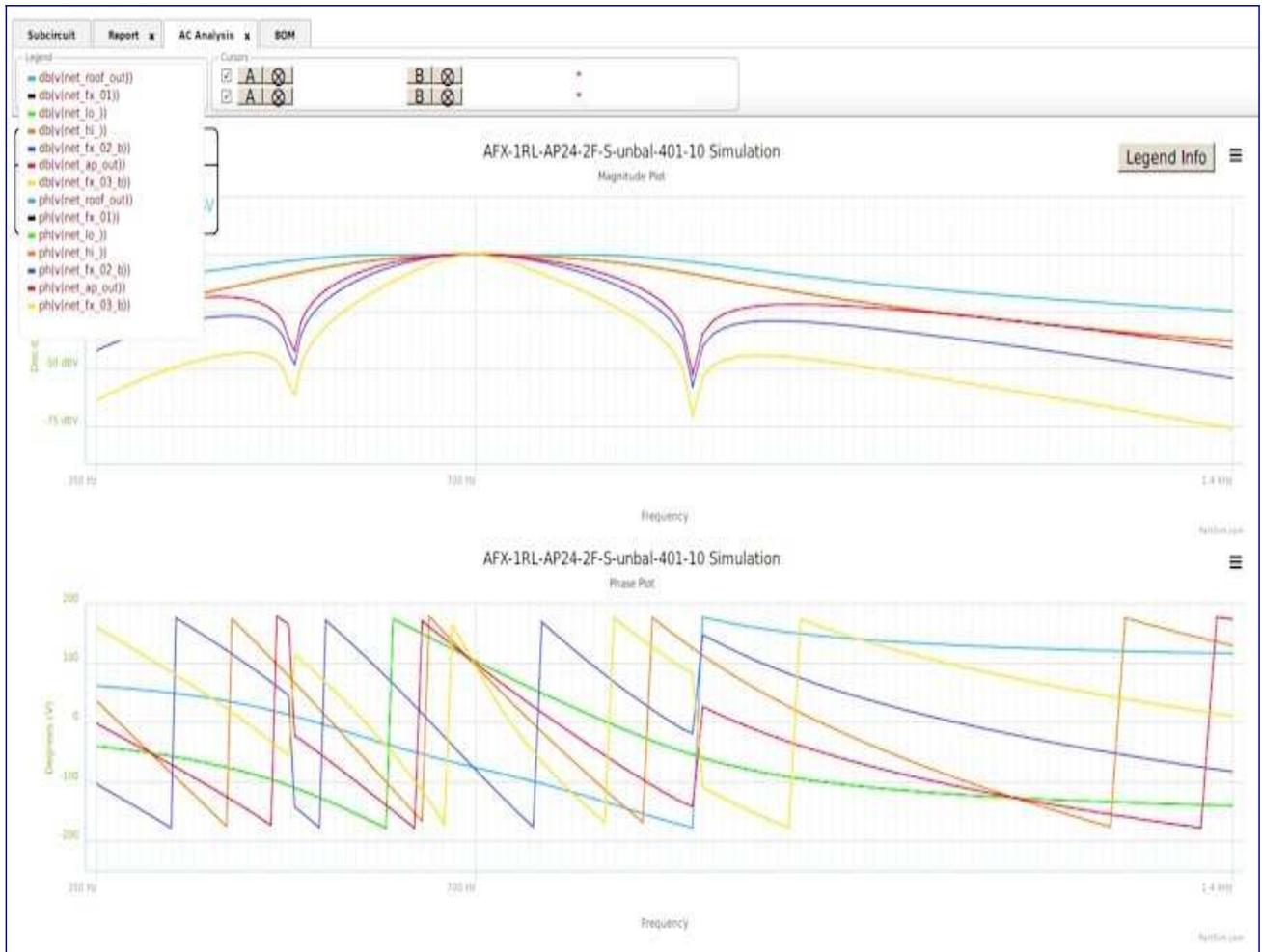
*** Notice: Fx-02 Q=3 and Fx-03 Q=10

are for extremely narrow Band-Pass, inside of Dual-Notches.



Magnitude Plot : AFC

- *** Below : **YELLOW** trace is final Q=20 result shown is the f(0) changed +\| to -3dB points.
- *** f(0) Shifts are confined to the AllPass Output plot.



Magnitude Plot : *** Magnitude Scale readings : V = -dB



*** Magnitude Scale readings : V = -dB
These Band-Pass signals-are NOT a Gaussian Shape.

- *** **Yellow** trace Filter-03 at Hi-Notch = -70 dB
- *** **Yellow** Spreads at the rate of 5.2 Hz per -dB attenuation (approx "**Brick-Wall**").

Circuit: **AFX_3RL-F8AFQ**

Special Advanced All-Pass Band-Pass circuit combining AFX and APC concepts.

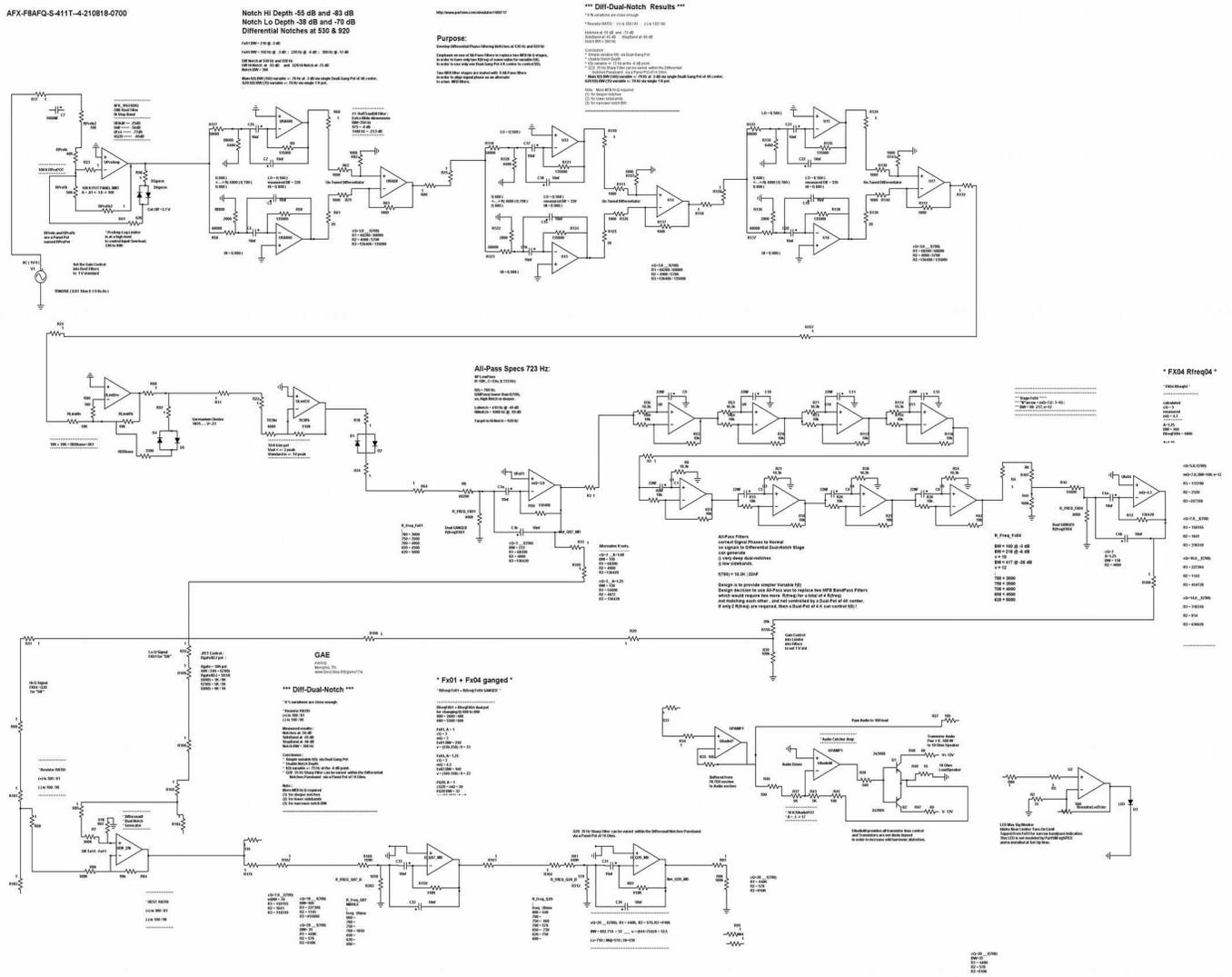
***** Two Variable MFB Filters**

with 8 All-Pass stages inserted in the middle

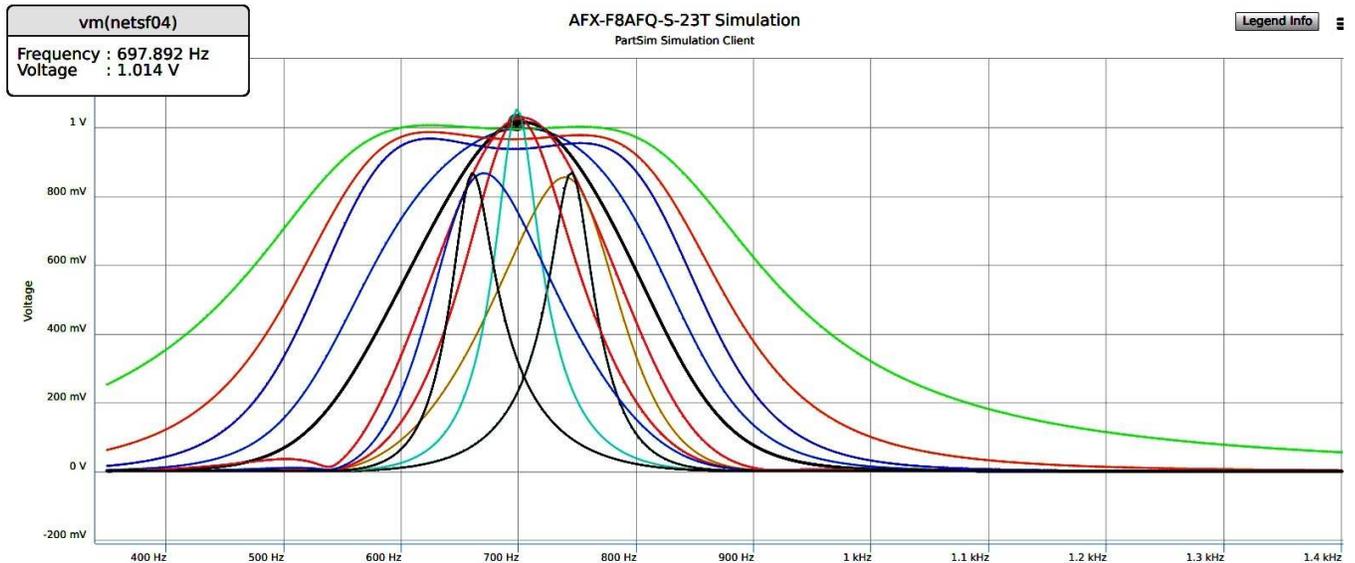
An effective combo-design, which is simpler

but not as effective as the AFX'V'-3RL-V4F-D-VQ version.

Result One Dual-Pot can control $f(0) \pm 75$ Hz, reading at the -3dB level.



Bode Plot : **AFX_3RL-F8AFQ**



Results: **AFX_3RL-F8AFQ with Dual-Notches.**

*** Compared to the AFX'V' ("AFV-3RL-V4F-D-VQ" version)

(1) BW @ -3dB is wider ;
160 Hz vs 90 Hz.

(2) Dual Notch BW is wider ; 380 Hz vs 330 Hz.
but the FX Q20 will narrow this to 35Hz.

(3) Variability of $f(0)$ is much narrower ; +/- 75 Hz is good (at -3dB),
vs +/- 100 Hz for the AFX'V' versions.

At $f(700 \text{ Hz})$, +/- 75 Hz is similar to +/- one piano note.

Changing the $f(0)$ of the All-Pass stages and/or the gain of AP stages

(1) will change the $f(0)$ of the AP notches up/dn factor of 2.

(2) will change the Band-Width of the notches w/n factor of 2..

$F(700)$ is best freq for the intended usage of this Filter Circuit ,
and is a compromise the author selected for this project.

(4) Variable $f(0)$ controlled physically
by a Single Panel-Mounted dual-gang Pot
is a good feature, even if not very much variation.

Magnitude Plot: **AFX_3RL-F8AFQ**

Magnitude Plot clearly shows the Notch Depth while shifting $f(0) \pm 100$ Hz

*** Notch Generator freq tracks with $f(0)$

*** at ± 100 Hz

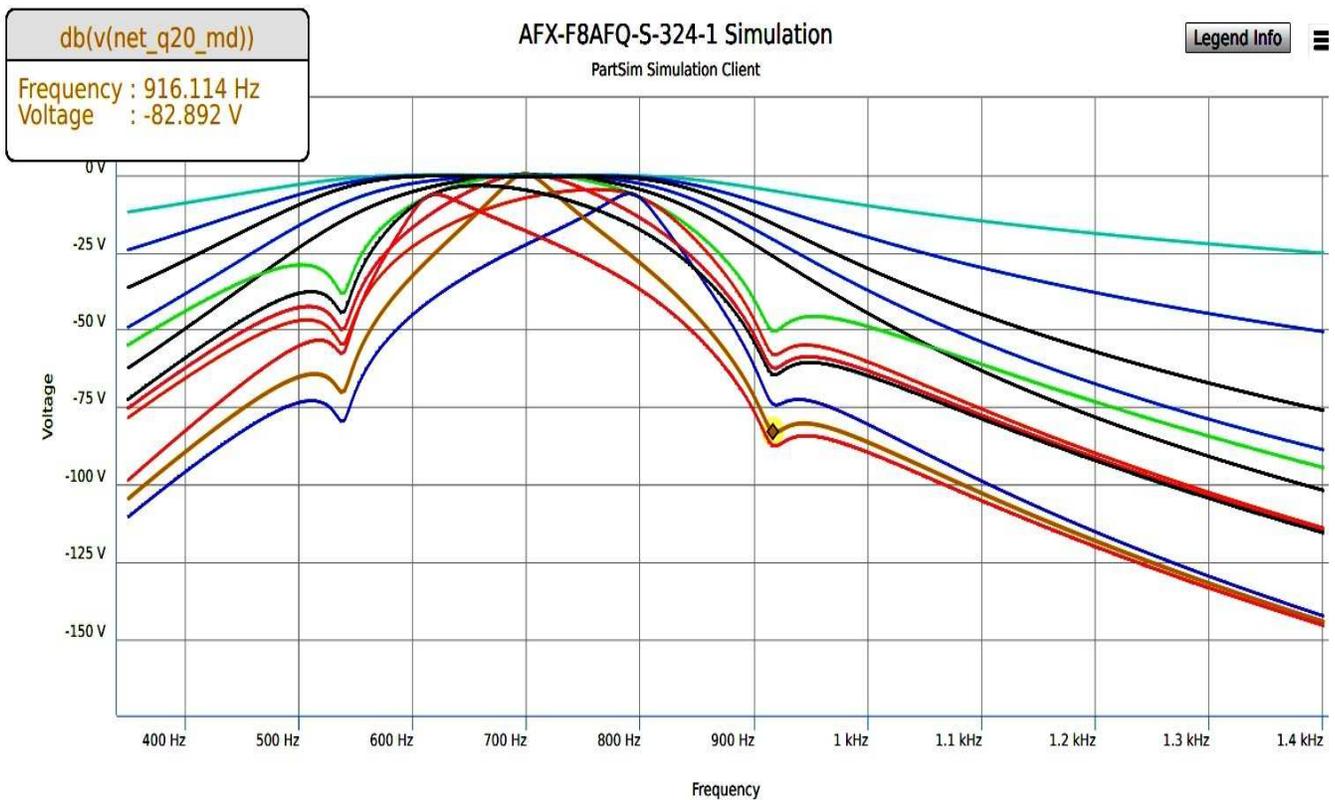
*** $F_x(100\text{Hz})$ is -0.5dB down

*** $F_x(35\text{Hz})$ is -1.0dB down

*** At $f(700)$ normal settings

Deep Notch (Yellow/Black trace)

is -82 dB 920Hz .



note:

*** Also authors explored the "UnBalanced" (7 Hz and 700 Hz) approach.

*** The All-Pass-Lo is tuned to 6.20 Hz (aprox. 7 Hz)

*** The All-Pass-Hi is tuned to 692 Hz. (aprox. 700 Hz)

*** Results: equal success in circuit performance.

*** Further experiments were done using the "UnBalanced" design

*** with $f(0)$ at 70, 137, 175, 350, 650 Hz vs. 750 Hz
to observe the patterns, with good results.

*** Further experiments were done using the "UnBalanced" design

*** with filter pairs of 2, 4, 6, 8, 10, 12, 14, 16, 18, 24
to observe the patterns ,with good results.

*** These circuits are not discussed in this paper.

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